

Correcting the heat load induced performance degradation on a XUV beamline

ACTOP08

Correcting the heat load induced performance degradation on a XUV beamline

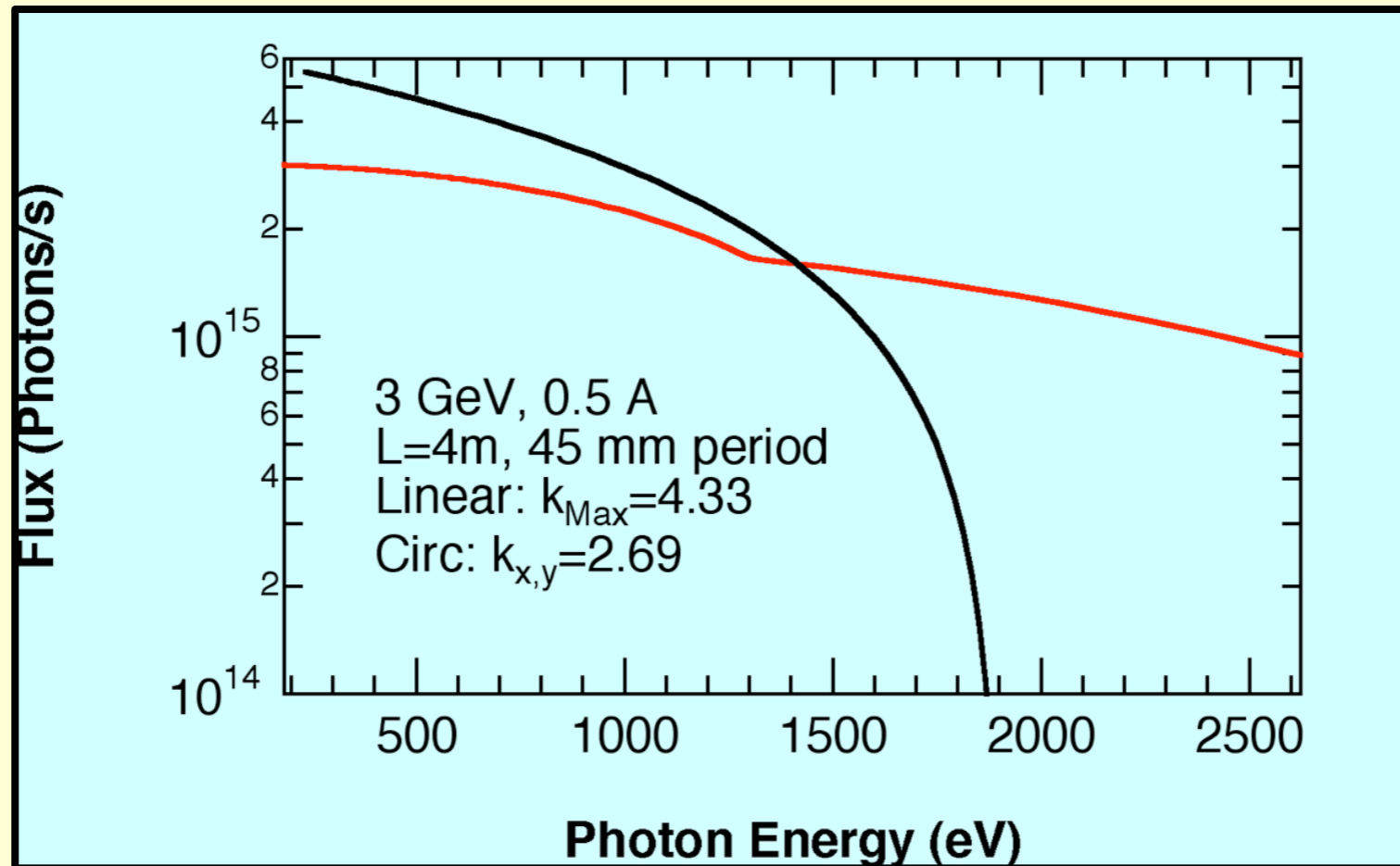
- ➔ Source
- ➔ Beamline Optical Design
- ➔ Ray Traces
- ➔ Resolution and Flux
- ➔ Heat Load
- ➔ Summary

Correcting the heat load induced performance degradation on a XUV beamline

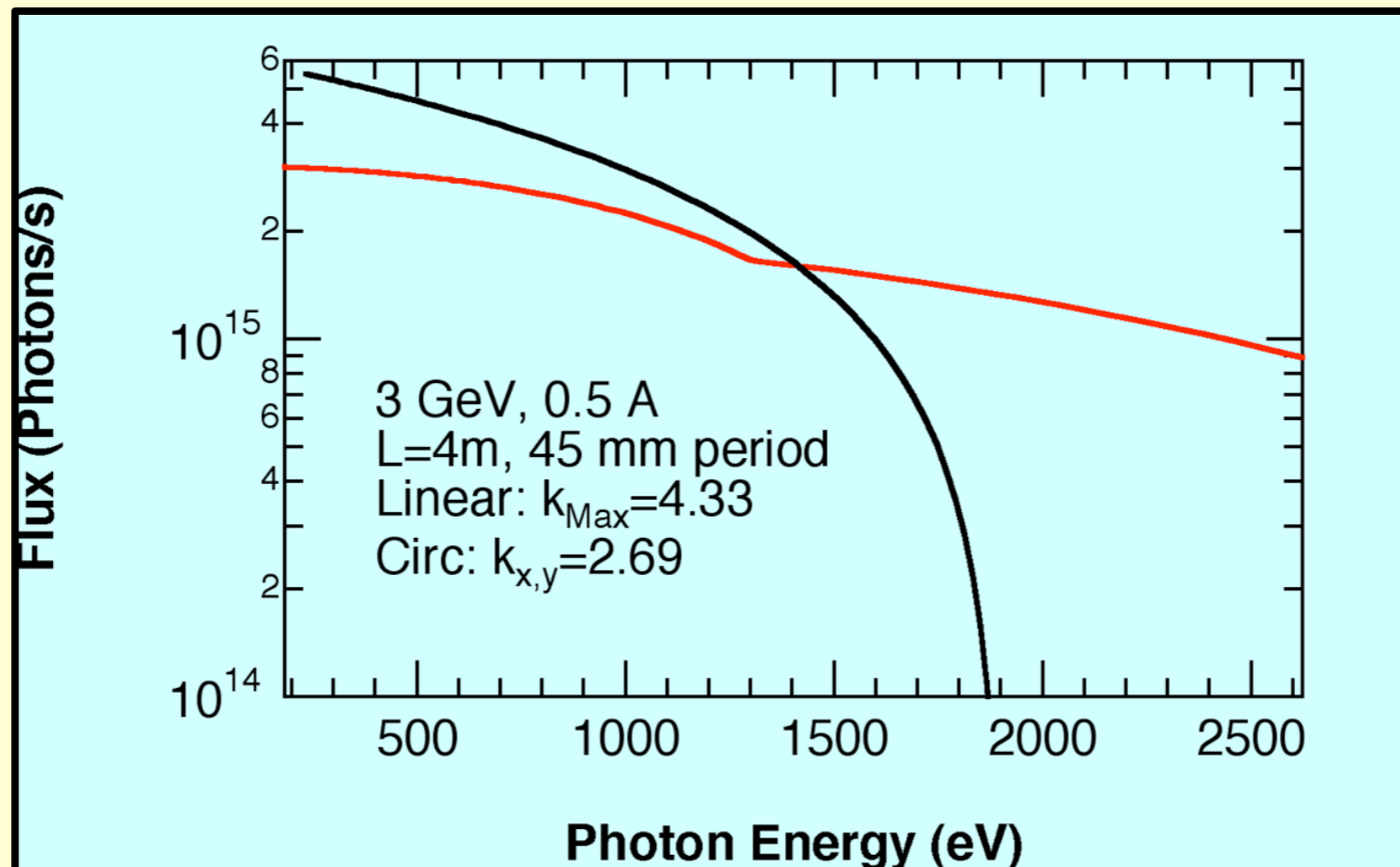
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S. Hulbert, NSLS
C. Sanchez-Henke, NSLS
D. Arena, NSLS
K. Kriesel, PSL
R. Reiningier, SAS-SRC

ACTOP08

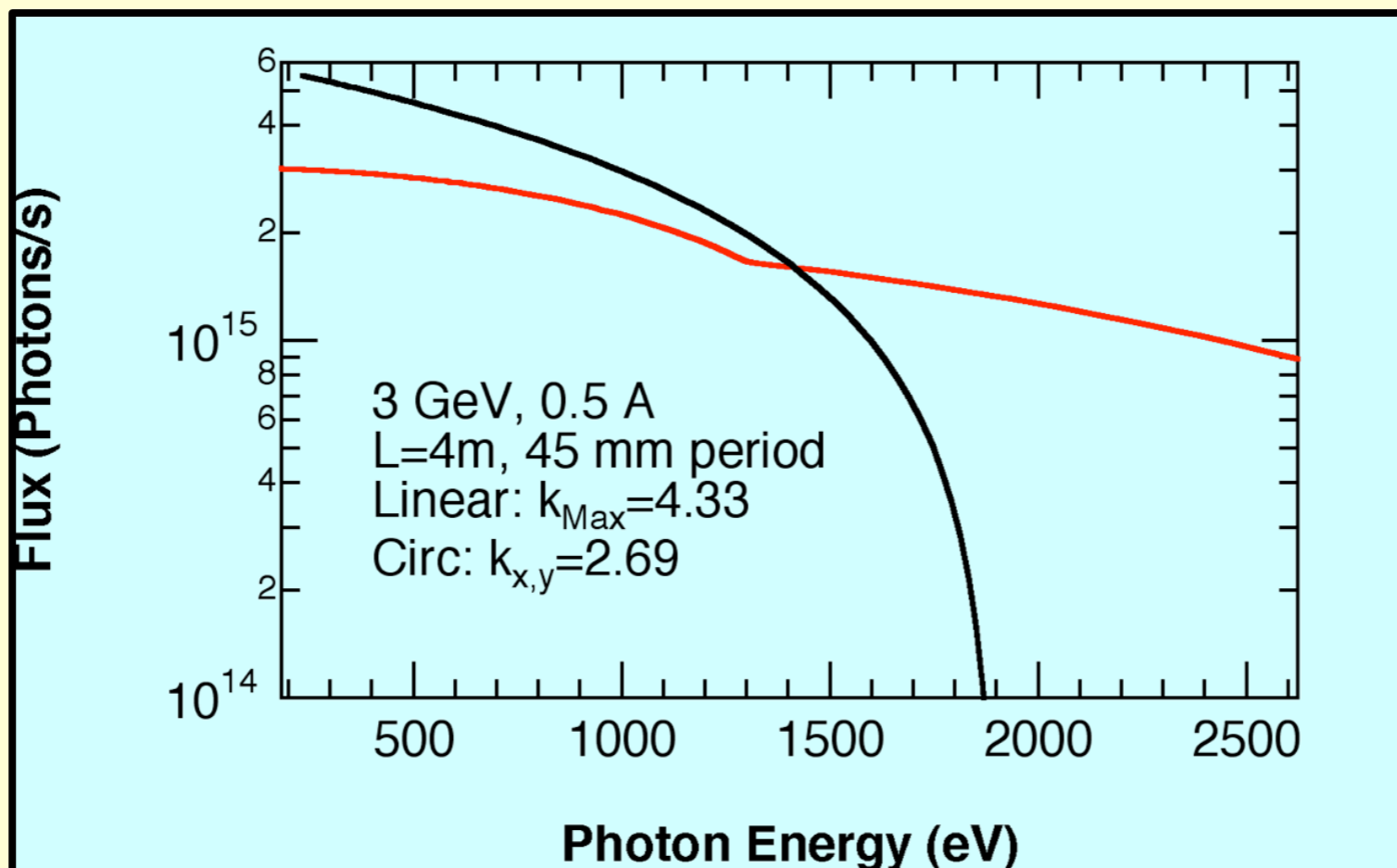


No need to focus horizontally



| | 200 eV | 1000 eV |
|--|--------|---------|
| $\sigma_{\text{hor}} (\mu\text{m})$ | 45 | 32 |
| $\sigma_{\text{ver}} (\mu\text{m})$ | 36 | 16 |
| $\sigma'_{\text{hor}} (\mu\text{rad})$ | 34 | 23 |
| $\sigma'_{\text{ver}} (\mu\text{rad})$ | 28 | 13 |

No need to focus horizontally



| | 200 eV | 1000 eV |
|-------------------------------------|--------|---------|
| σ_{hor} (μm) | 45 | 32 |
| σ_{ver} (μm) | 36 | 16 |
| σ'_{hor} (μrad) | 34 | 23 |
| σ'_{ver} (μrad) | 28 | 13 |

200 eV at 50 m, $\sigma=1.7$ mm

No need to focus horizontally

$$k(w) = k_0(1 + 2b_2 w + 3b_3 w^2 \dots)$$

$$f_{20} = \frac{\cos^2 \alpha}{r_1} + \frac{\cos^2 \beta}{r_2} + 2b_2 n k \lambda$$

$$f_{30} = \sin \alpha \frac{\cos^2 \alpha}{r_1^2} + \sin \beta \frac{\cos^2 \beta}{r_2^2} + 2b_3 n k \lambda$$

Collimated beam $r_1 \rightarrow \infty$

$$k(w) = k_0(1 + 2b_2 w + 3b_3 w^2 \dots)$$

$$f_{20} = \frac{\cos^2 \alpha}{r_1} + \frac{\cos^2 \beta}{r_2} + 2b_2 n k \lambda$$

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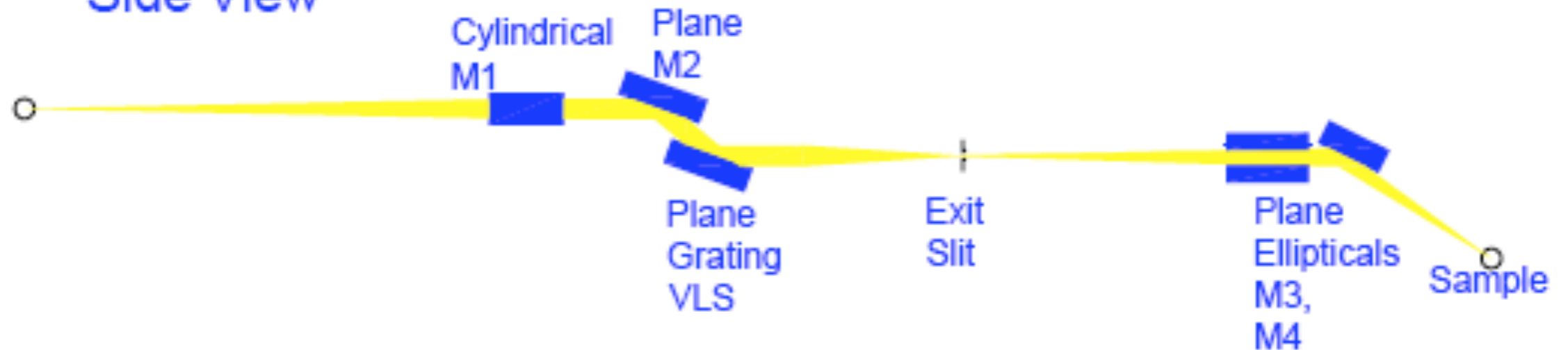
Collimated beam $r_1 \rightarrow \infty$

$$\text{PM: } \gamma = \frac{\alpha - \beta}{2} \Rightarrow f_{20} = 0, n k \lambda = \sin \alpha + \sin \beta$$

$$c = \frac{\cos \beta}{\cos \alpha}$$

Beamline

Side View



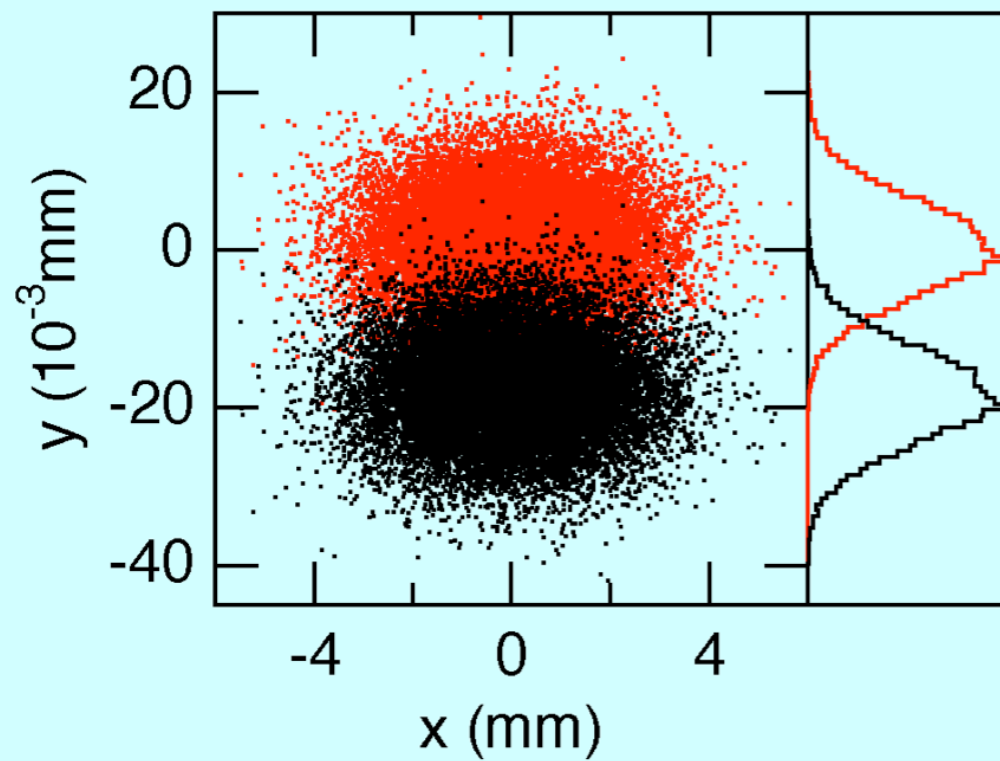
Horizontal Focusing: M3, 25 demagnification

| Element | Distance (mm) | Angle (°) | Deflection | $4\sigma \times 4\sigma$ (mm ²) |
|-----------------------|--------------------|-------------------|------------|---|
| M1- Sagittal Cylinder | 29500 | 88.75 | Horizontal | 190×3.5 |
| M2- Plane | 31929 ^a | 84.0 ^a | Vertical | 380(70)×5 |
| Gr - Grating | 32000 ^a | 86.2 ^a | Vertical | 180×5 |
| Slit | 42000 | | | |
| M3 - Plane Elliptical | 43200 | 88.75 | Horizontal | 280×1 |
| M4 - Plane Elliptical | 43950 | 88.75 | Vertical | 48×4 |
| Sample | 44950 | | | |

^a For 183 eV

Ray Traces at Slit, 183 eV

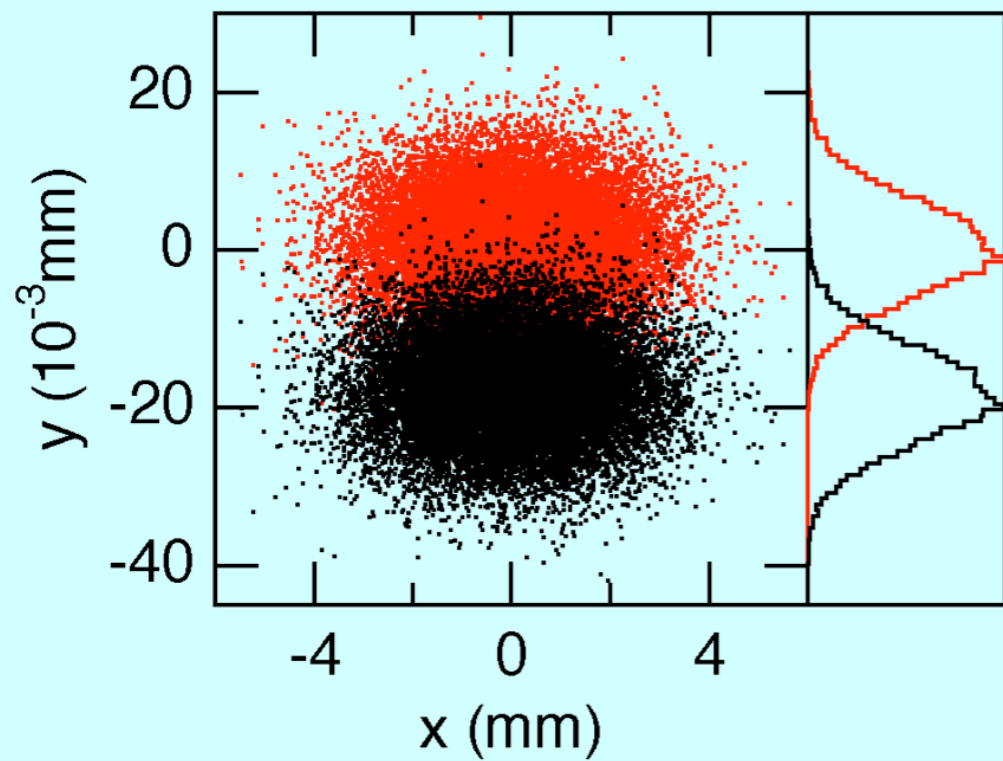
Slit, SE:0.02", HEG 183.00 eV, **183.006 eV**
 $\sigma_x: 1.5$ $\sigma_y: 0.006$



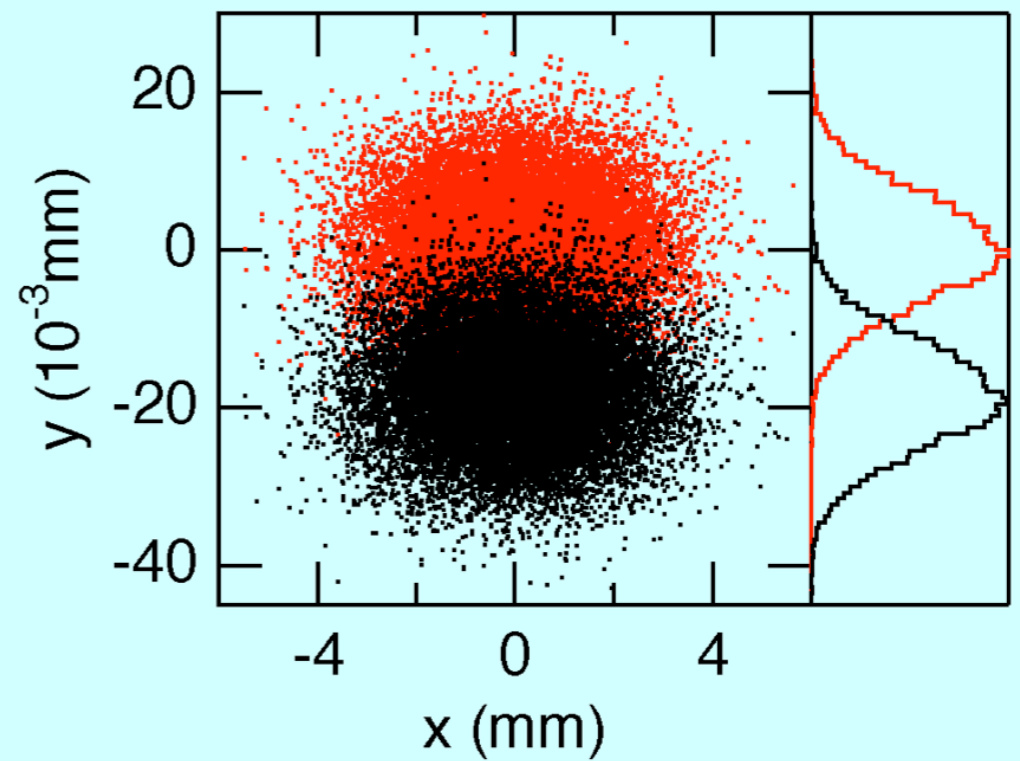
RP >30000

Ray Traces at Slit, 183 eV

Slit, SE:0.02", HEG 183.00 eV, **183.006 eV**
 $\sigma_x: 1.5$ $\sigma_y: 0.006$



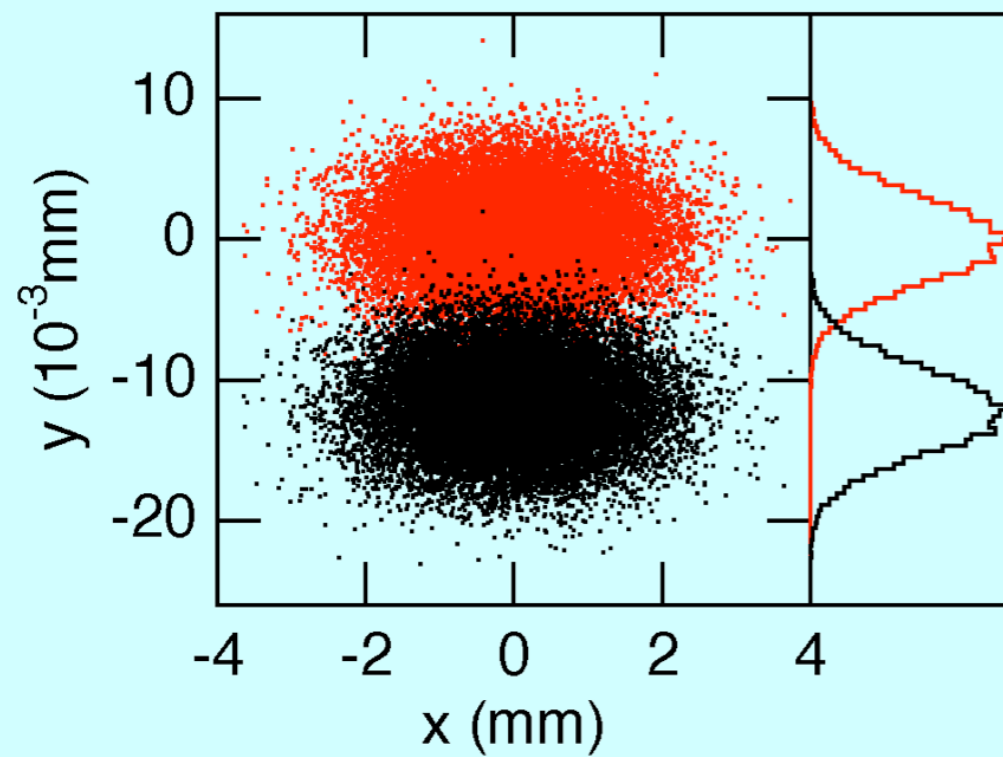
Slit, SE:0.04", HEG 183.00 eV, **183.006 eV**
 $\sigma_x: 1.5$ $\sigma_y: 0.007$



RP >30000

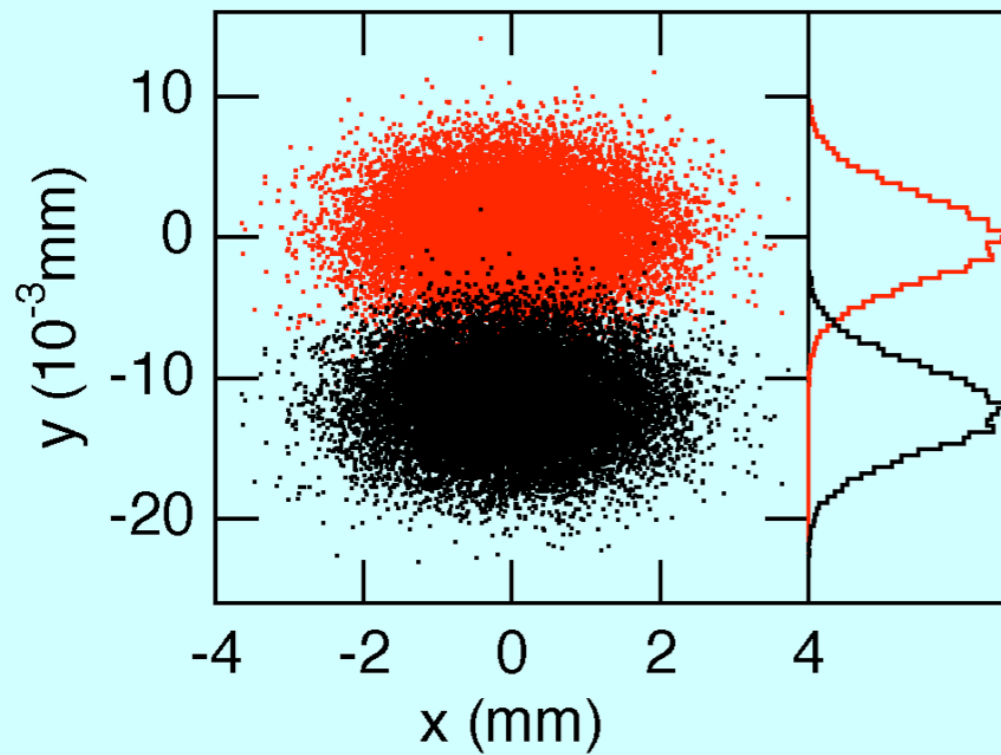
Ray Traces at Slit, 1000 eV

Slit, SE:0.02", HEG 1000.00 eV, 1000.05 eV
 $\sigma_x: 0.98$ $\sigma_y: 0.003$

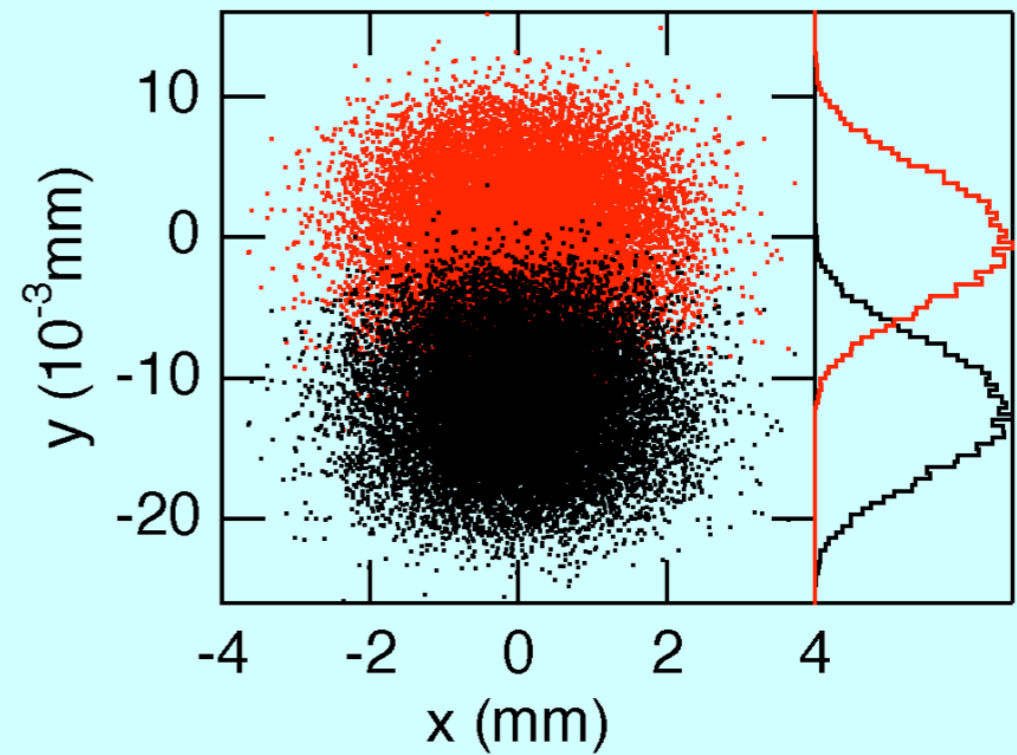


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Slit, SE:0.02", HEG 1000.00 eV, 1000.05 eV
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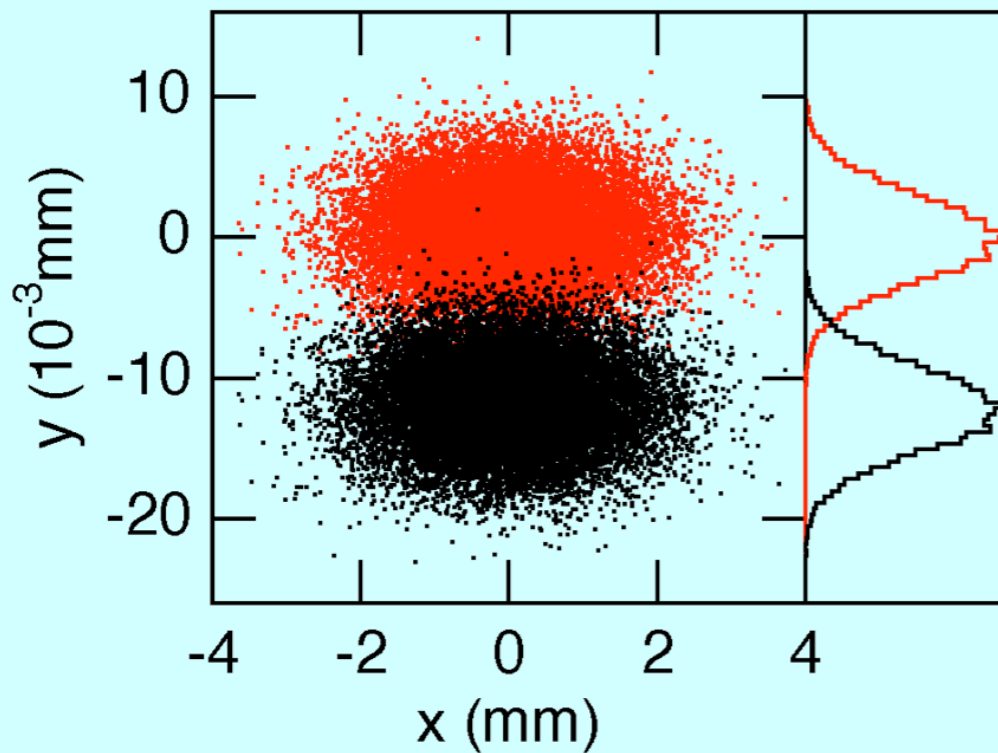


Slit, SE:0.04", HEG 1000.00 eV, 1000.05 eV
 $\sigma_x: 0.98$ $\sigma_y: 0.0042$

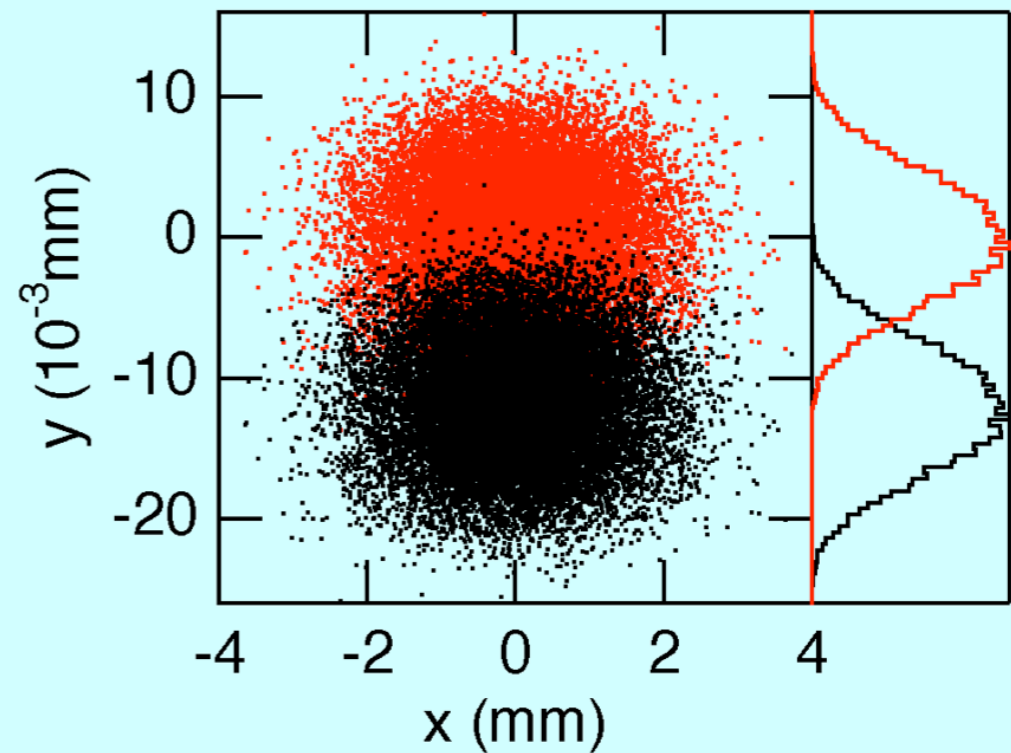


Ray Traces at Slit, 1000 eV

Slit, SE:0.02", HEG 1000.00 eV, 1000.05 eV
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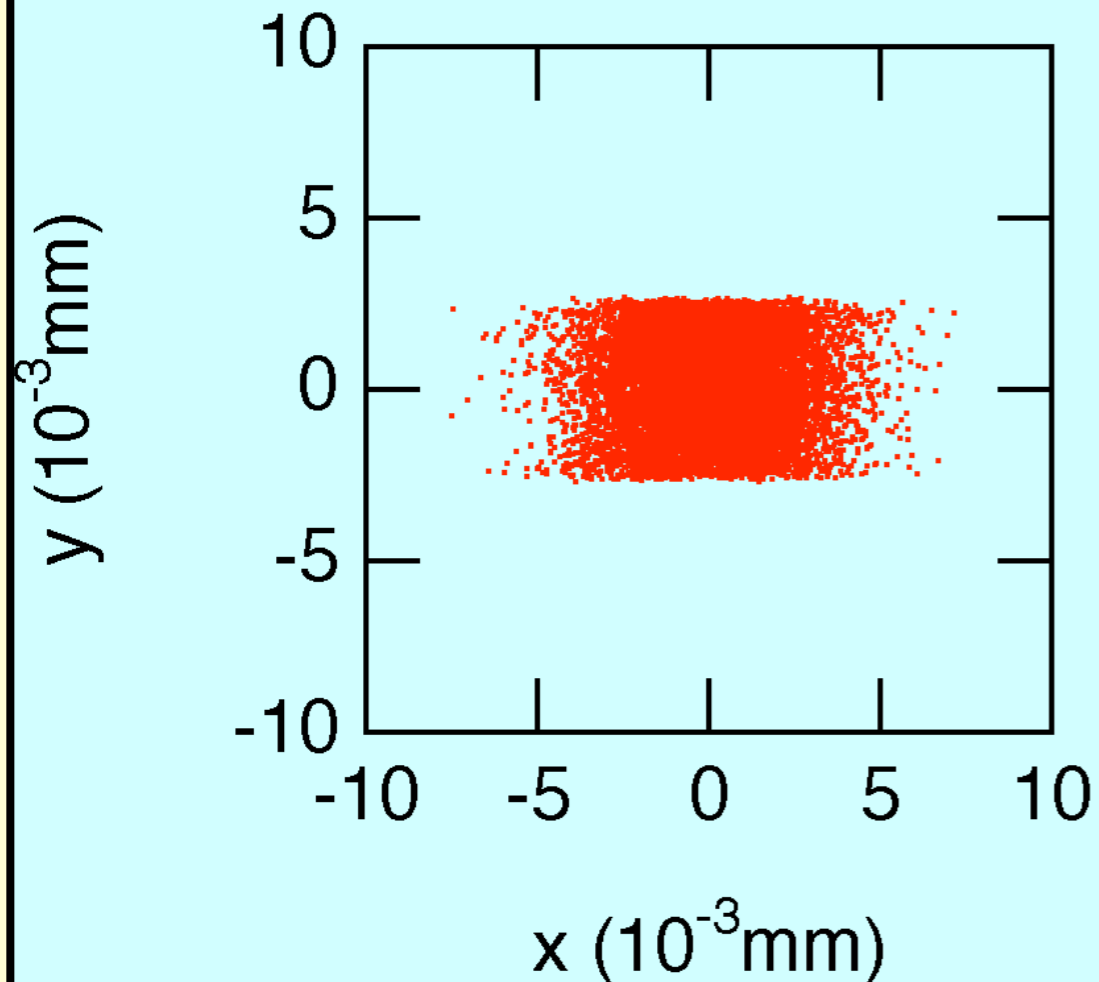


RMS Slope Errors $\approx 0.02''$

Size at Sample

230 eV, HEG, Linear, 10 μm slit

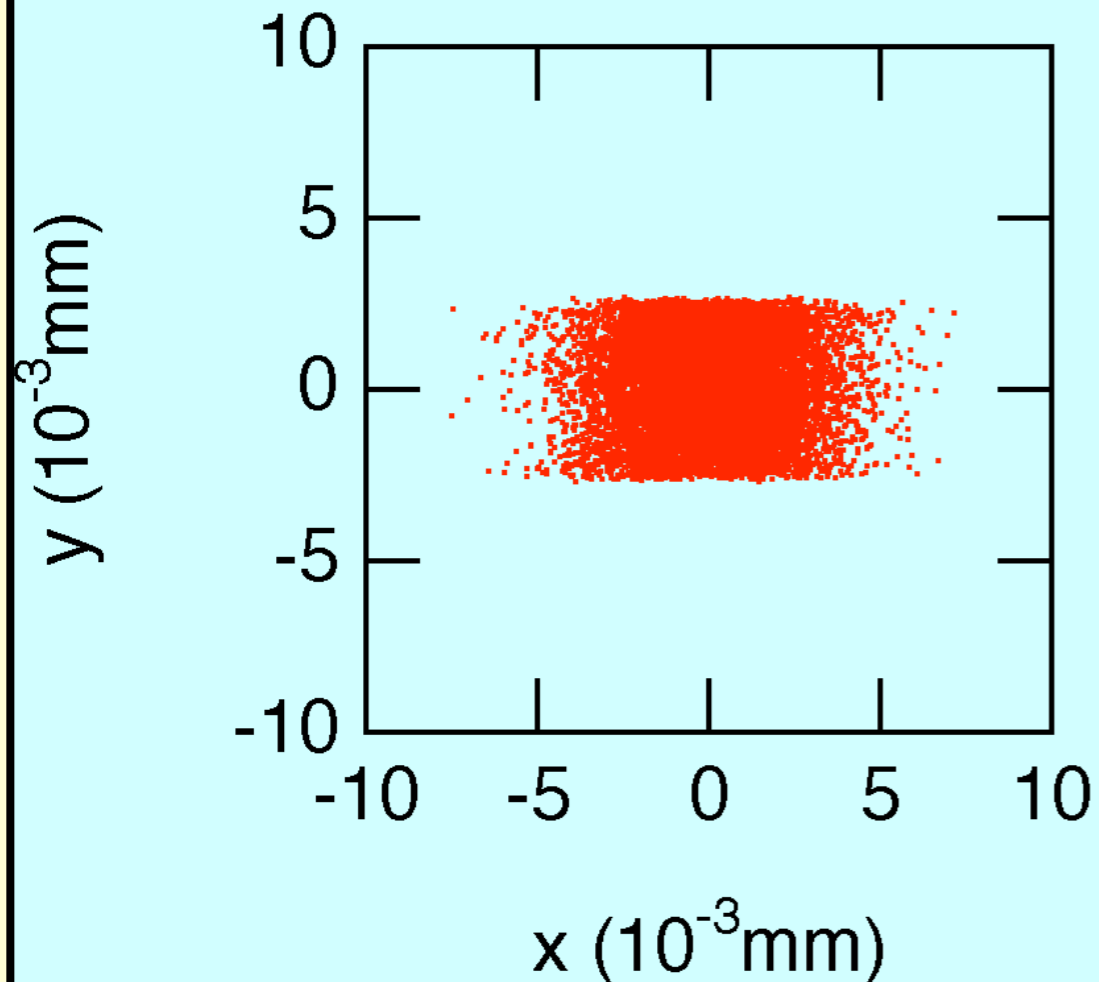
Sample, 230 eV HEG, No SE
 $\sigma_x: 1.9 \mu\text{m}$ $\sigma_y: 1.4 \mu\text{m}$



Size at Sample

230 eV, HEG, Linear, 10 μm slit

Sample, 230 eV HEG, No SE
 $\sigma_x: 1.9 \mu\text{m}$ $\sigma_y: 1.4 \mu\text{m}$

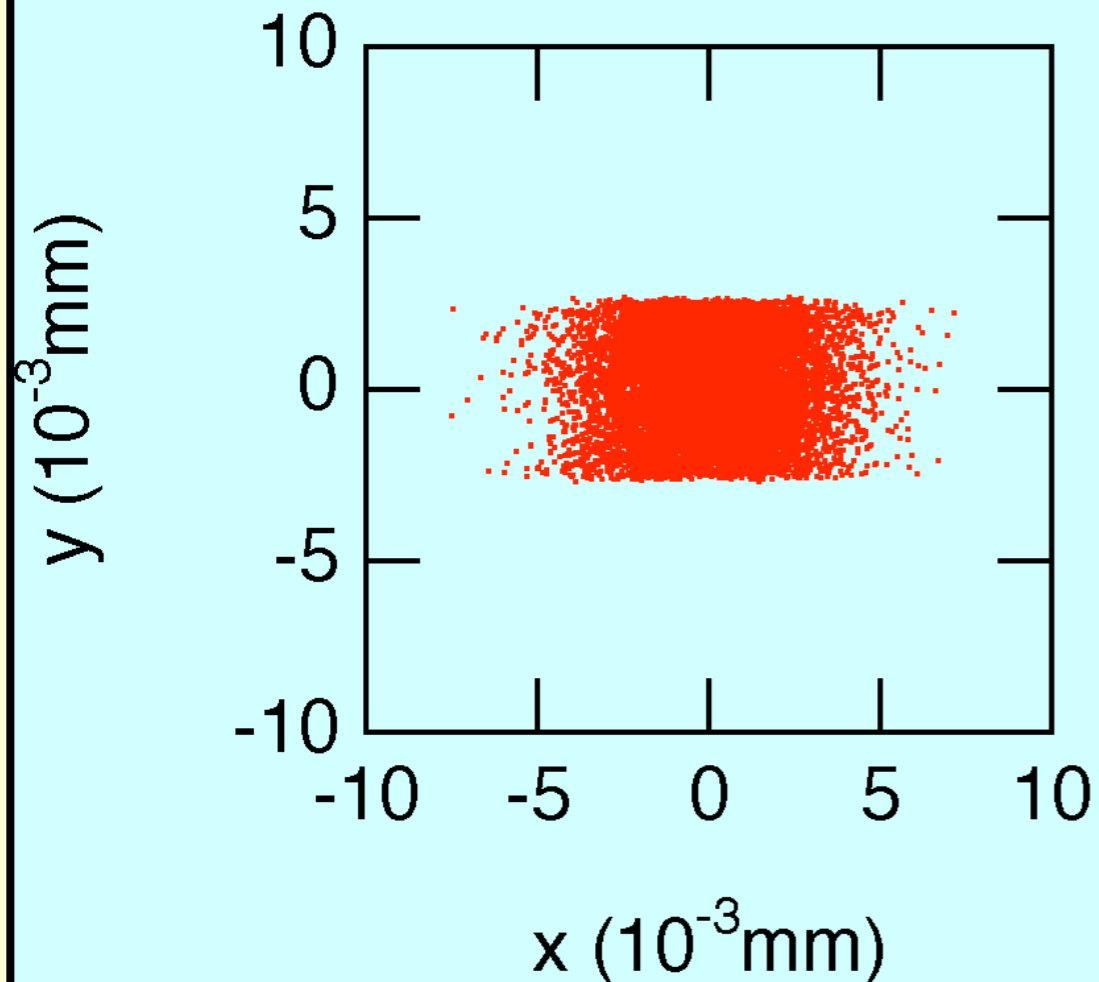


SE 0.1" meridional M1, M3, M4

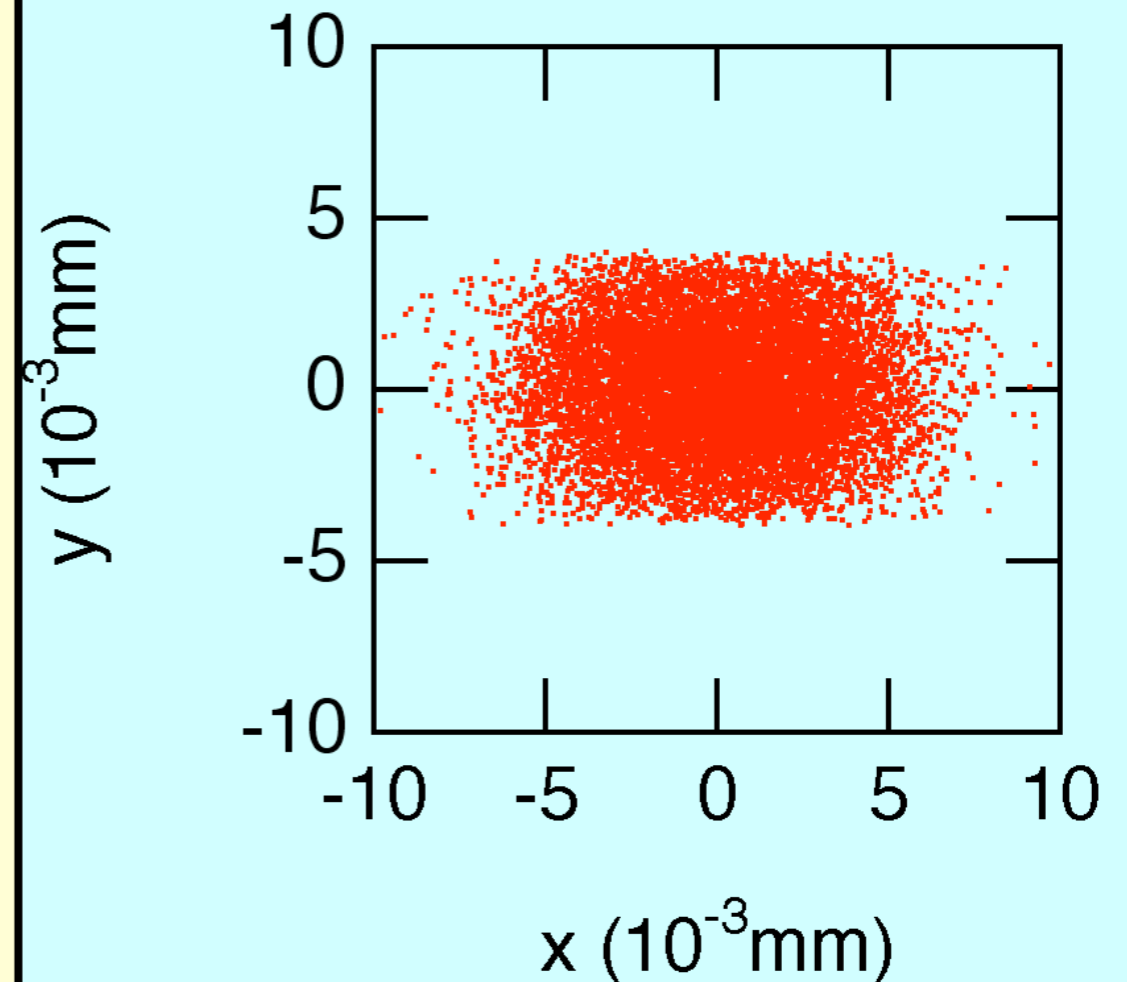
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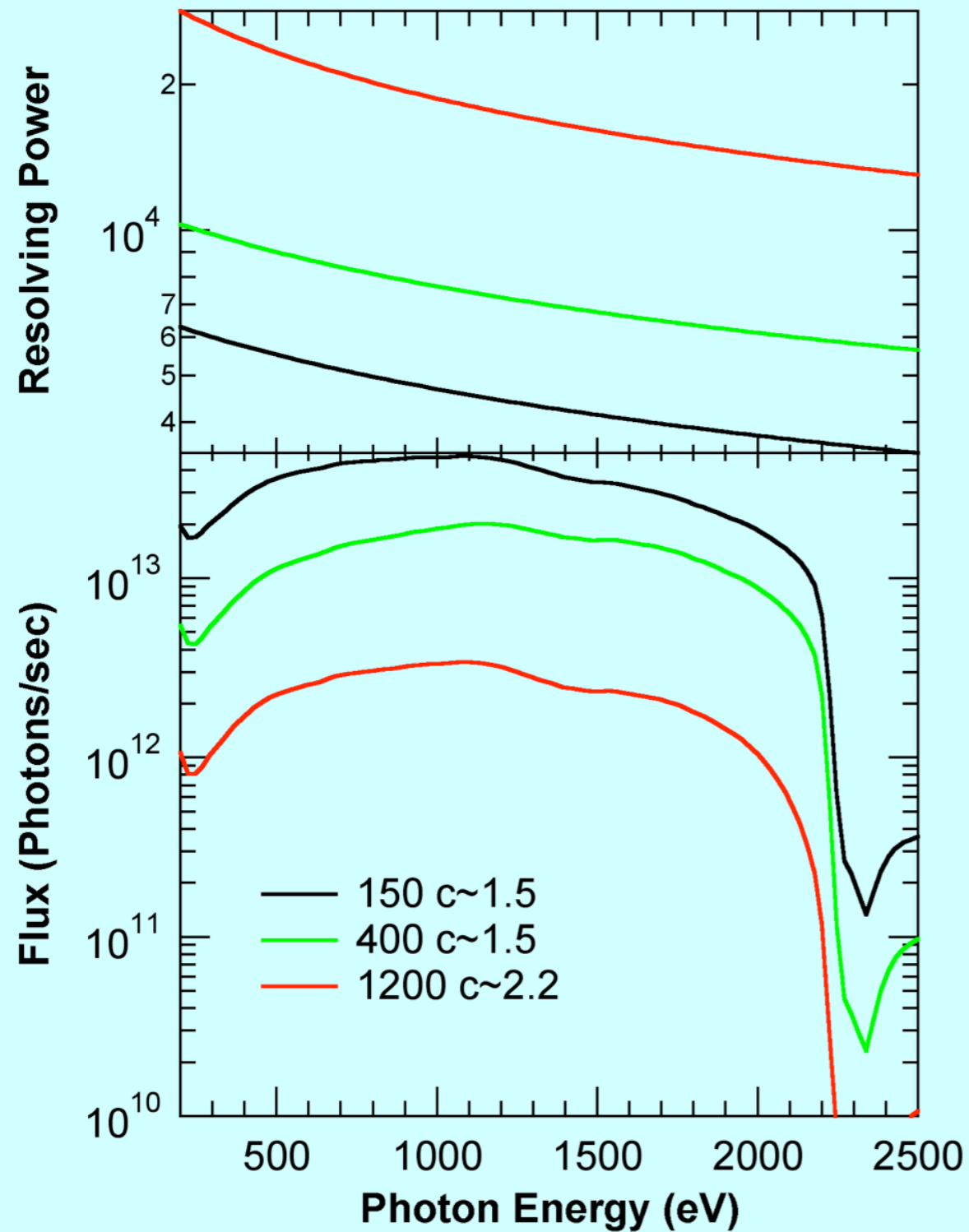
Sample, 230 eV HEG, SE
 $\sigma_x: 2.8 \mu\text{m}$ $\sigma_y: 1.7 \mu\text{m}$



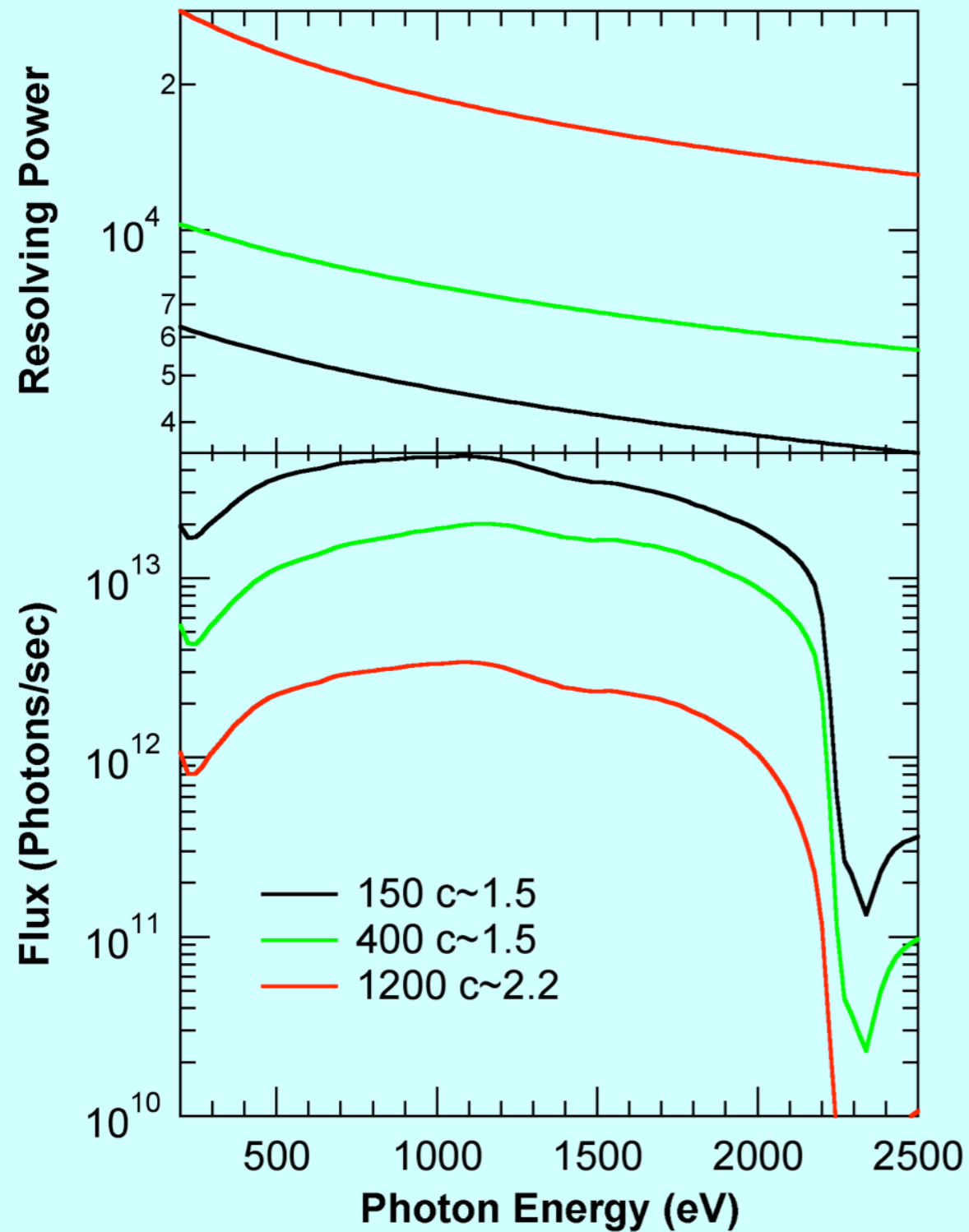
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Resolution & Flux (linear)

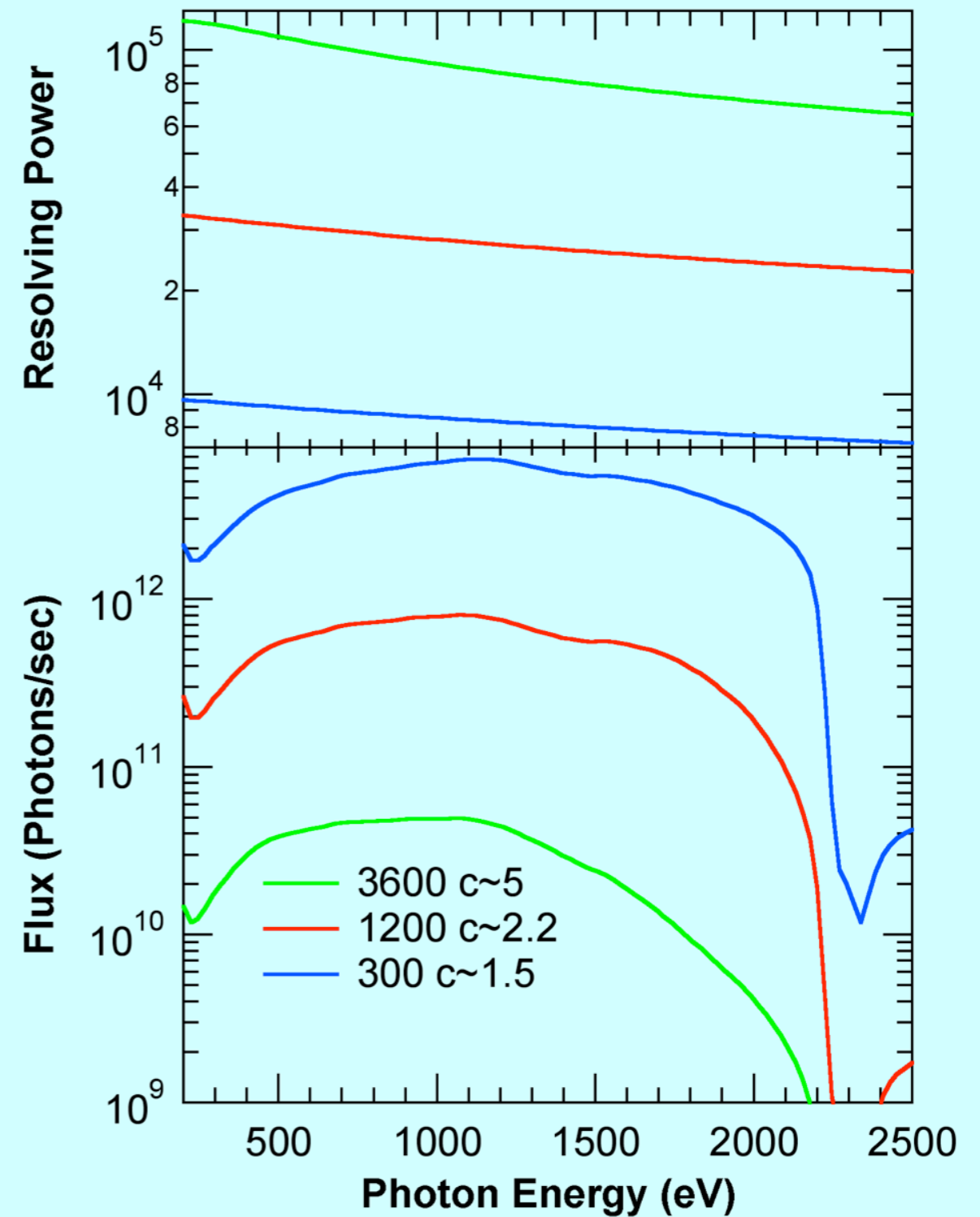
Source, Grating efficiencies, Reflectivity, 10 μm Slit, Slope errors.



Resolution & Flux (linear)

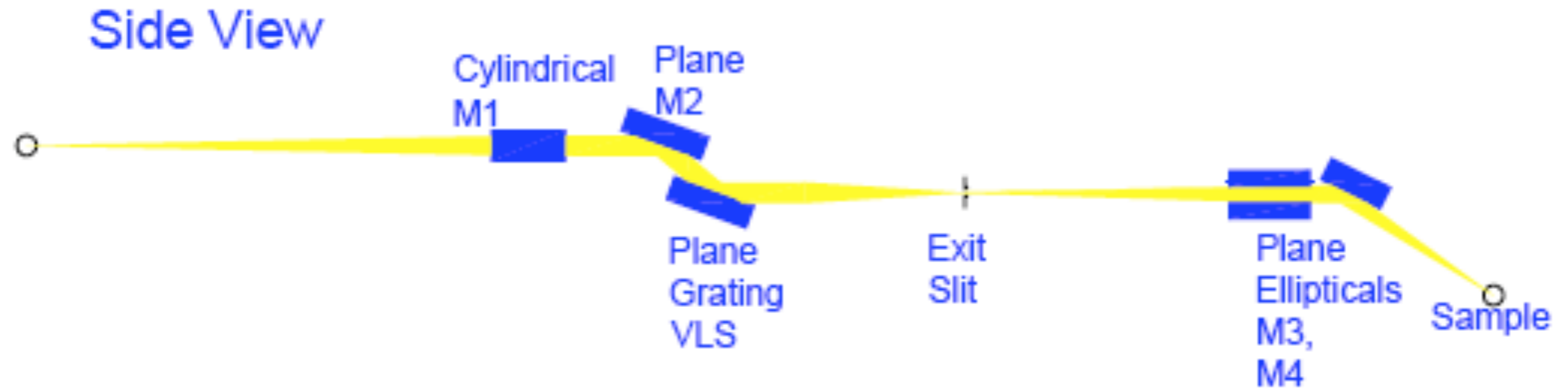


20 m Grating-Slit, 5 μm slit



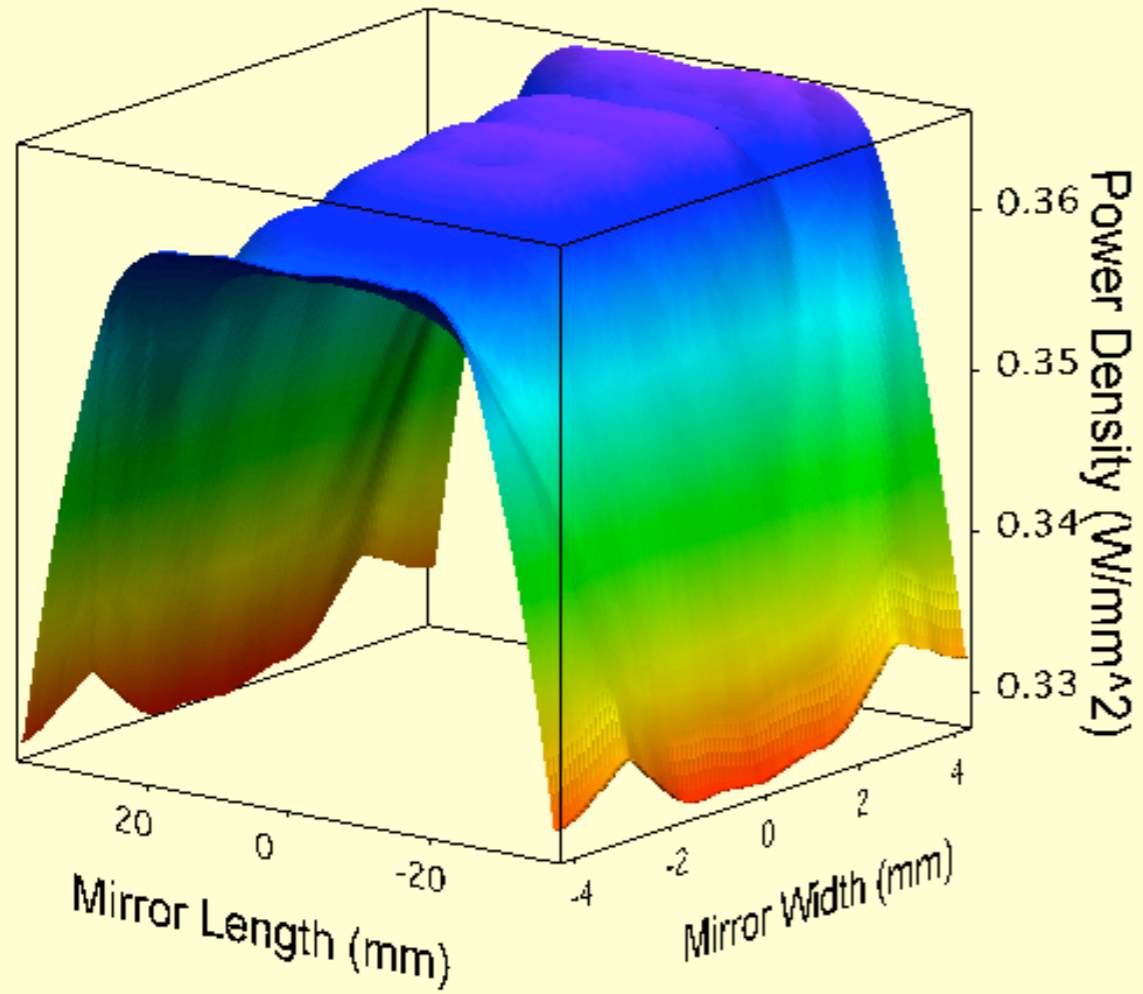
Heat Load Deformation Correction

- ➔ 3 GeV, 0.5 A
- ➔ Linear mode: 12 kW total at 183 eV
- ➔ 0.27×0.27 mrad² only 2.15 kW
- ➔ 1.9 kW absorbed on M1. Deformation \Rightarrow blow up horizontal at sample
- ➔ 0.24 kW on M2 \Rightarrow Resolution



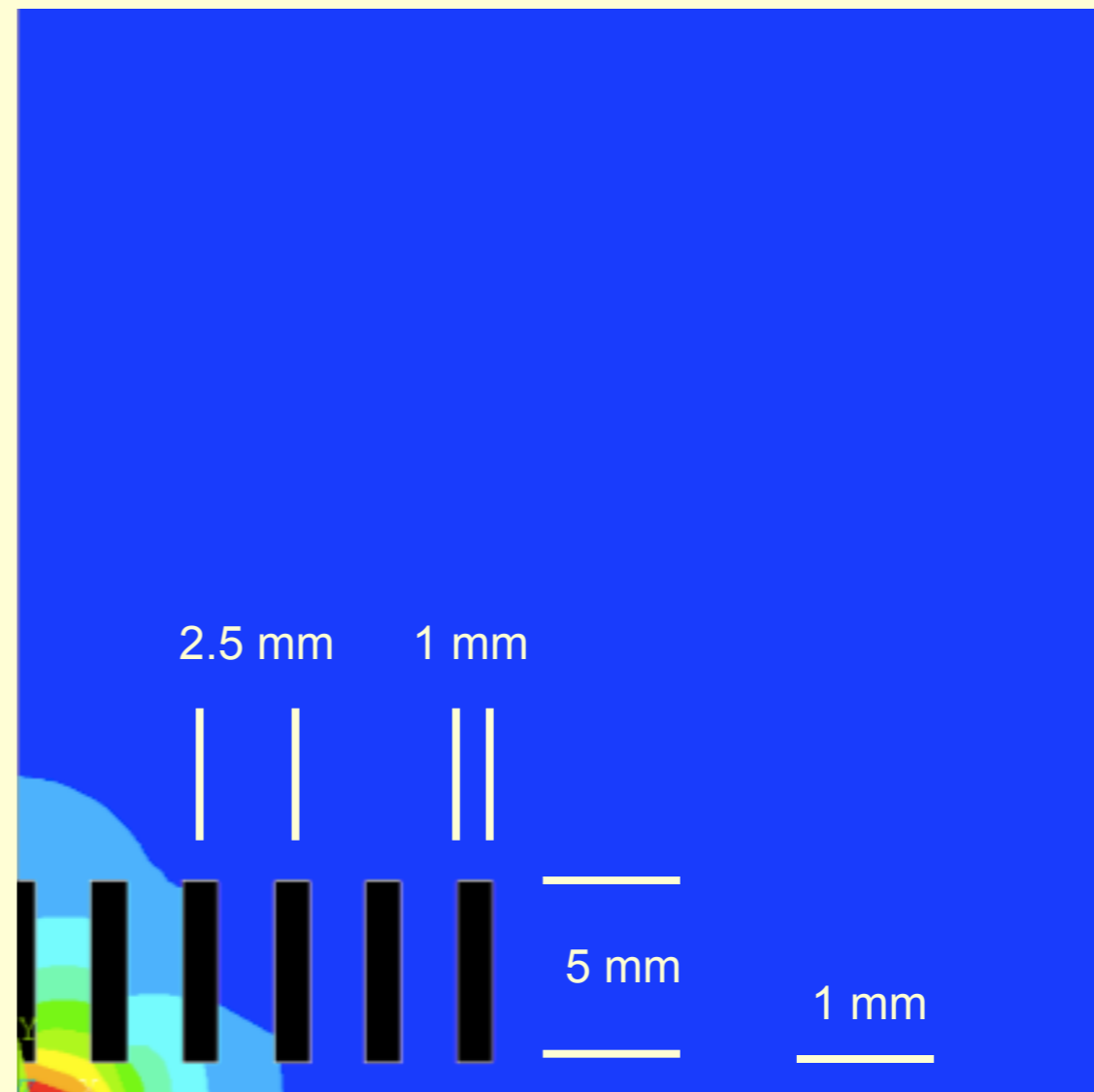
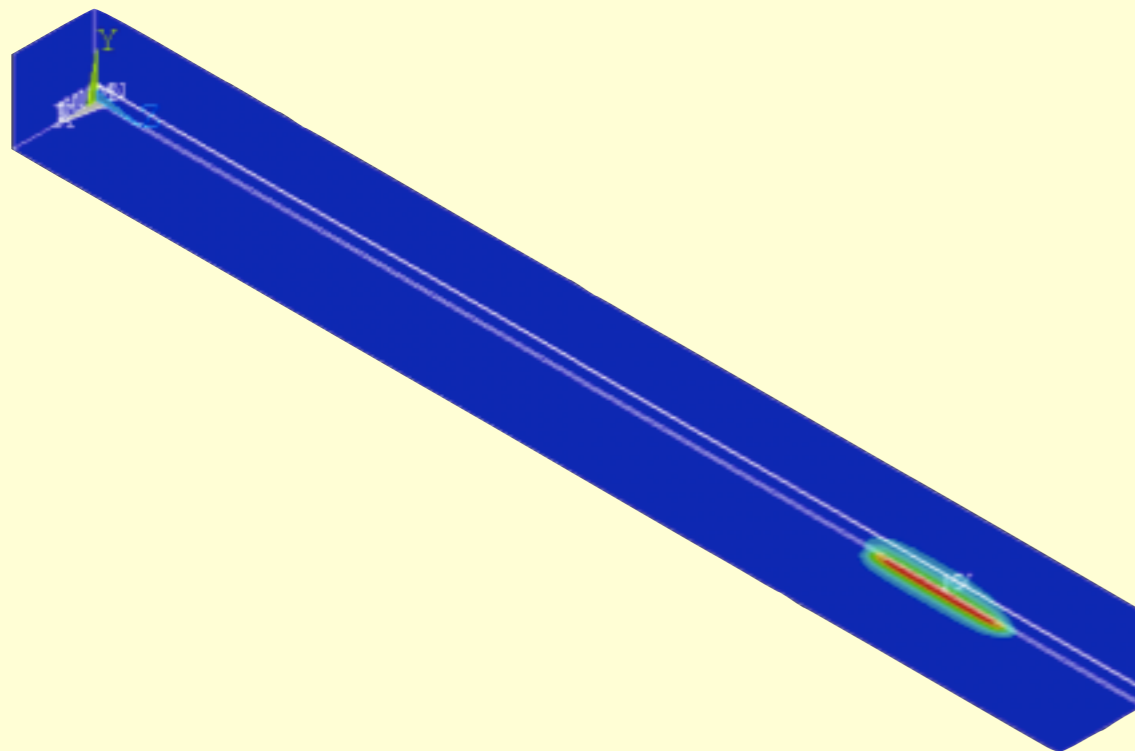
Power on M2

➔ Total absorbed 236 W



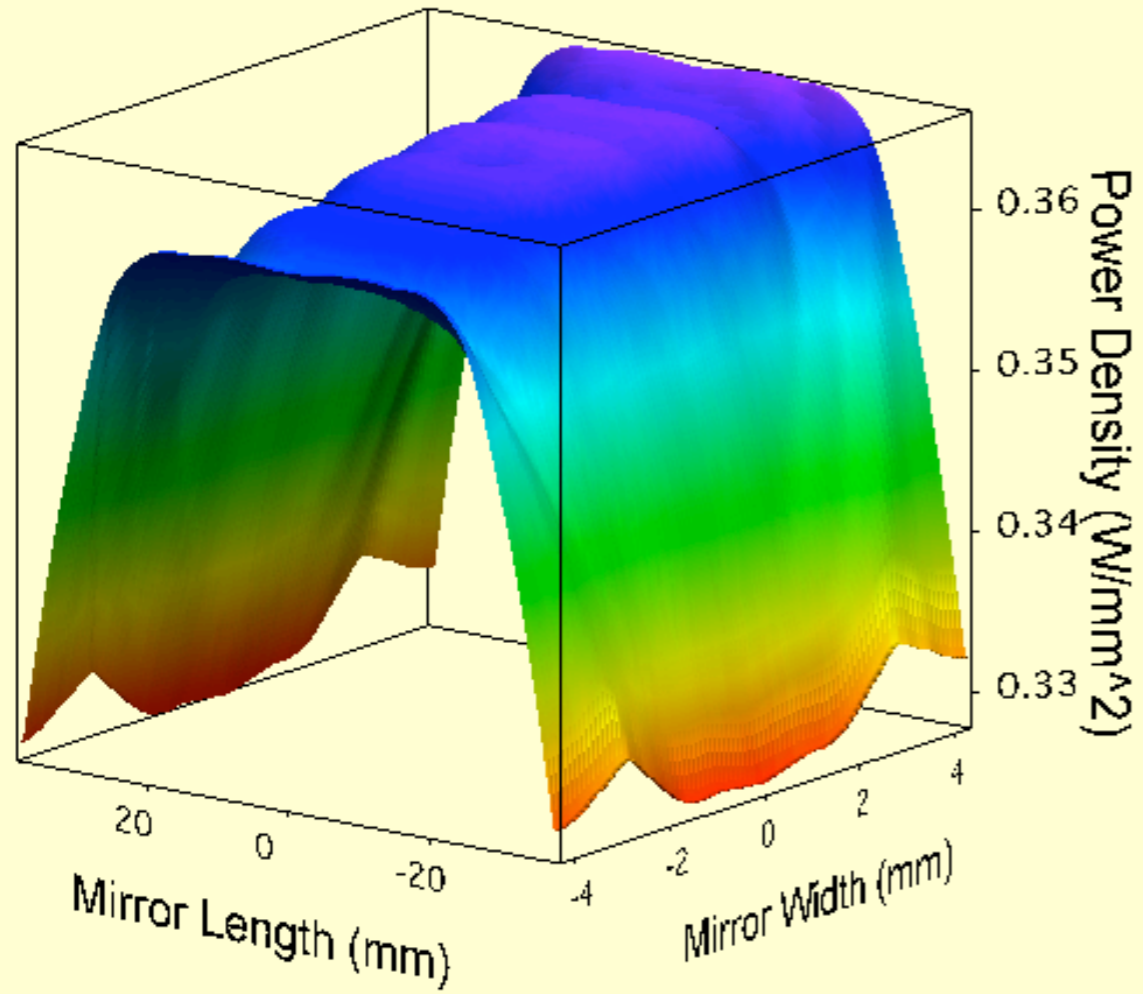
Finite Element Analysis, M2

| Parameters used FEA, SC Si | |
|---|---------------------------------|
| Density (g/mm ³) | 2.3310 ⁻³ |
| Young Modulus (N/mm ²) | 1.3105 |
| Poisson's ratio | 0.28 |
| CTE (ppm/°C) | -0.33 to 3.25 over 100 to 400K |
| Conductivity, <i>K</i> (W/mm/K) | 0.913 to 0.105 over 100 to 400K |
| Water Bulk Temp (°C) | 20 |
| Convection coeff., (W/mm ² /C) | 0.01 |



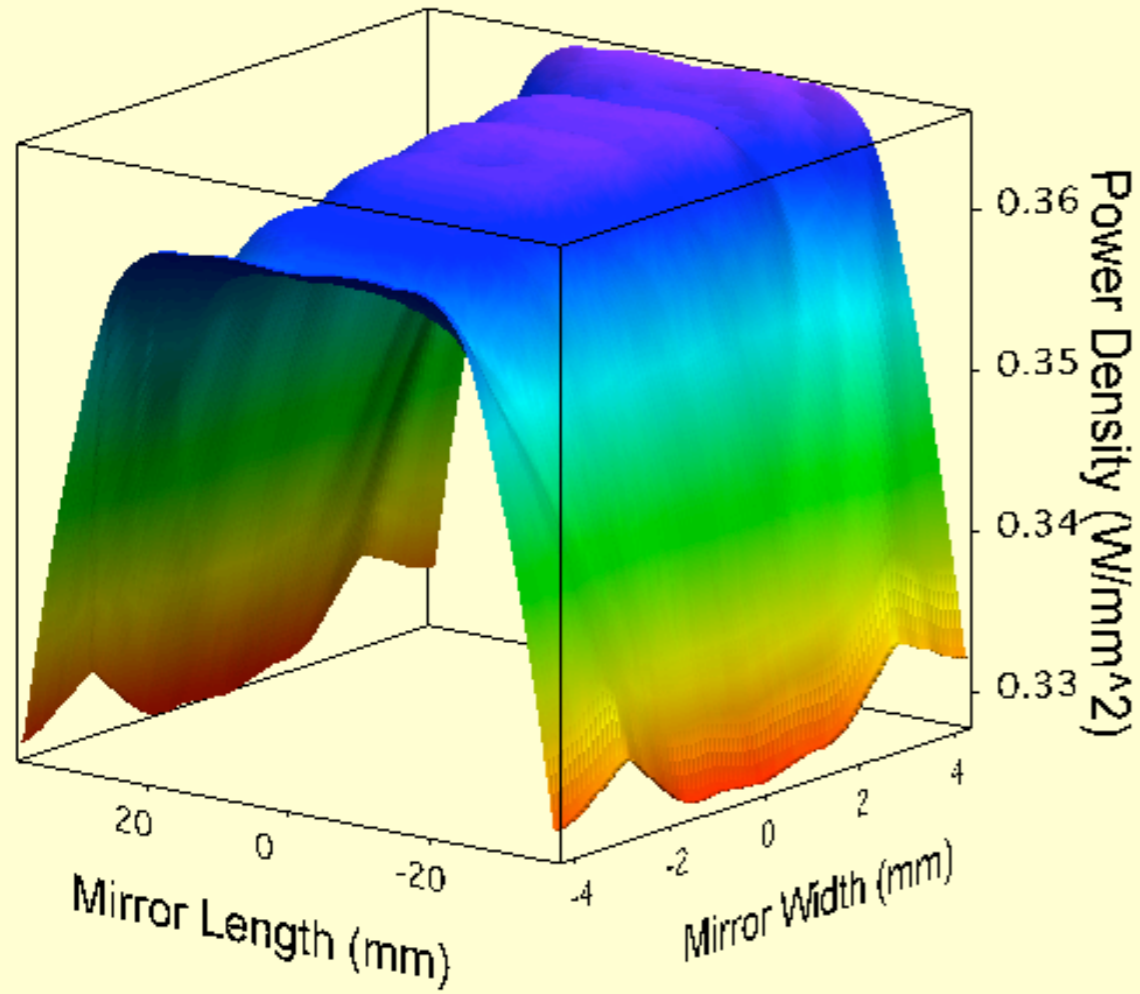
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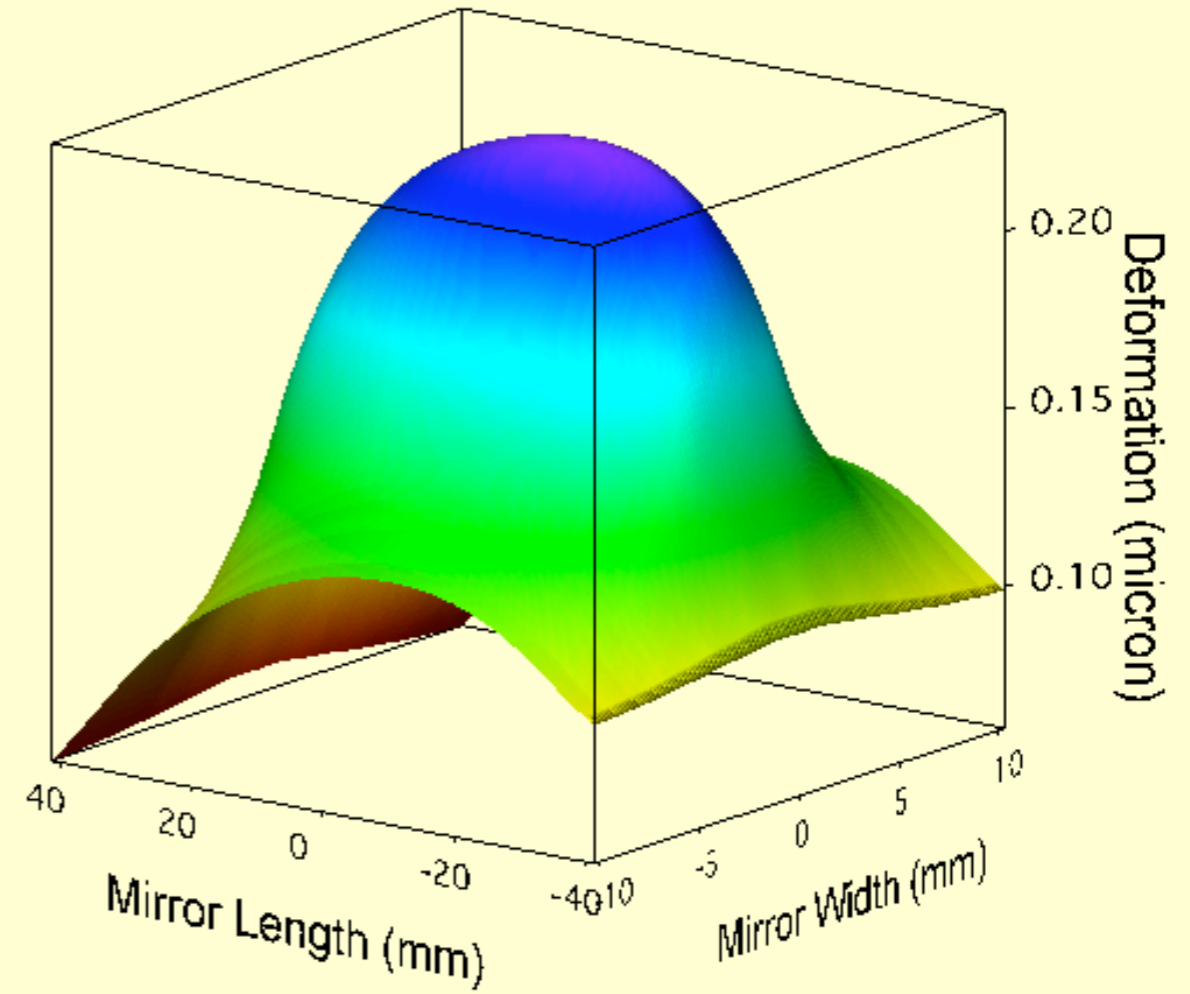


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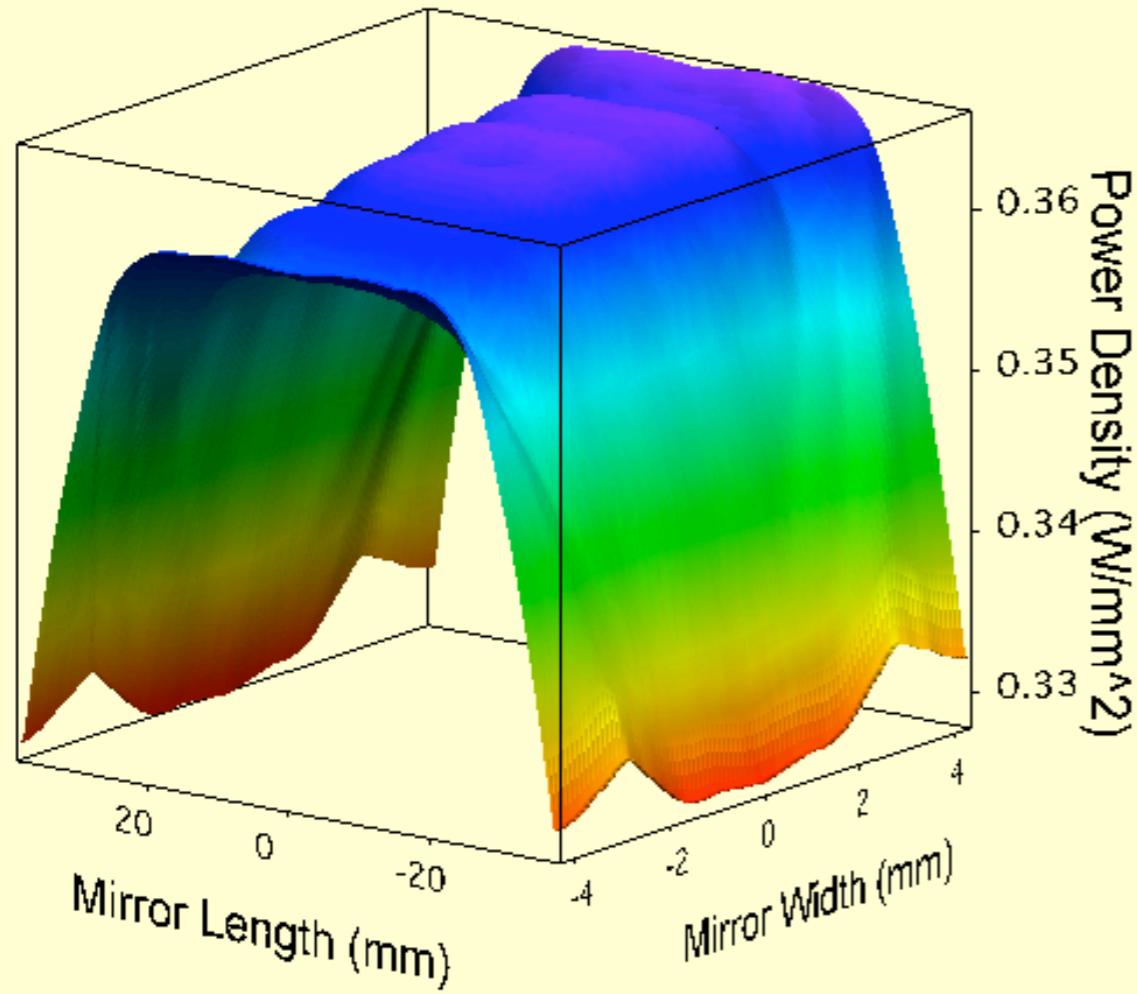


➔ Internally water cooled

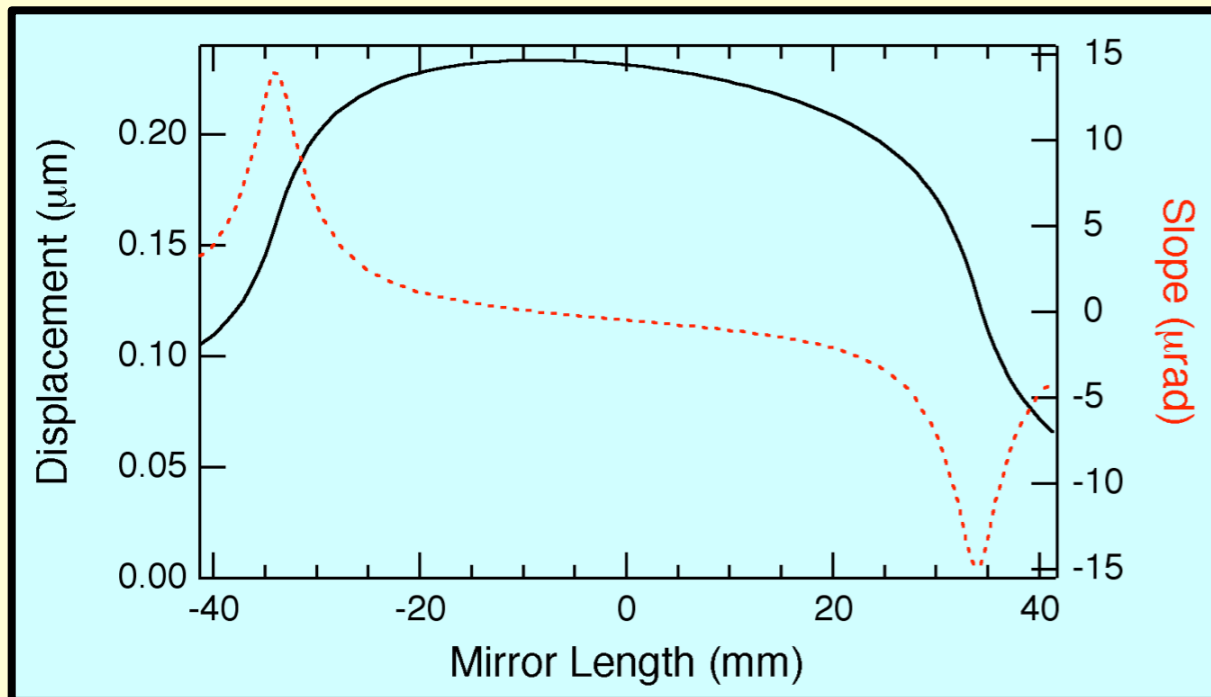
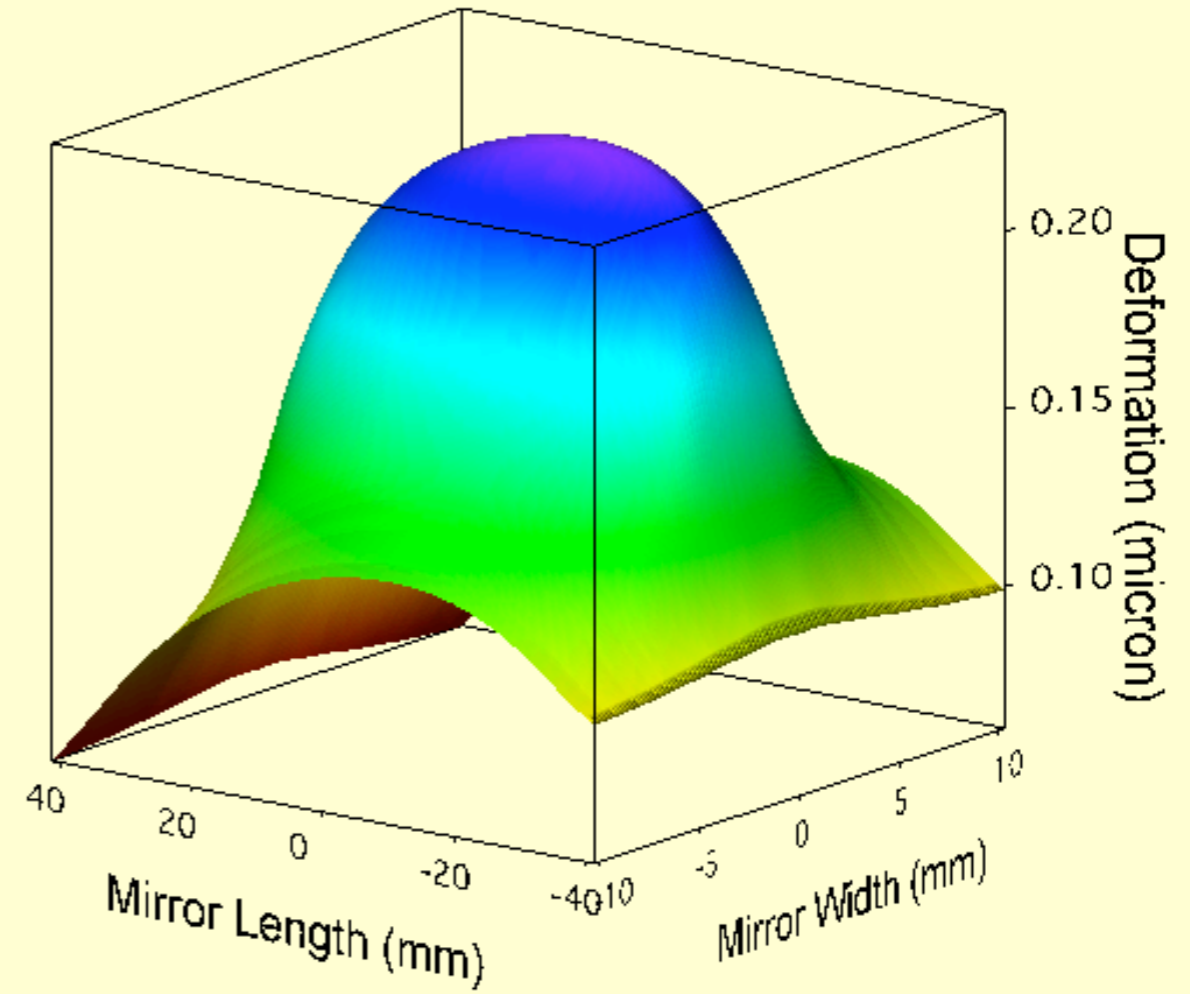


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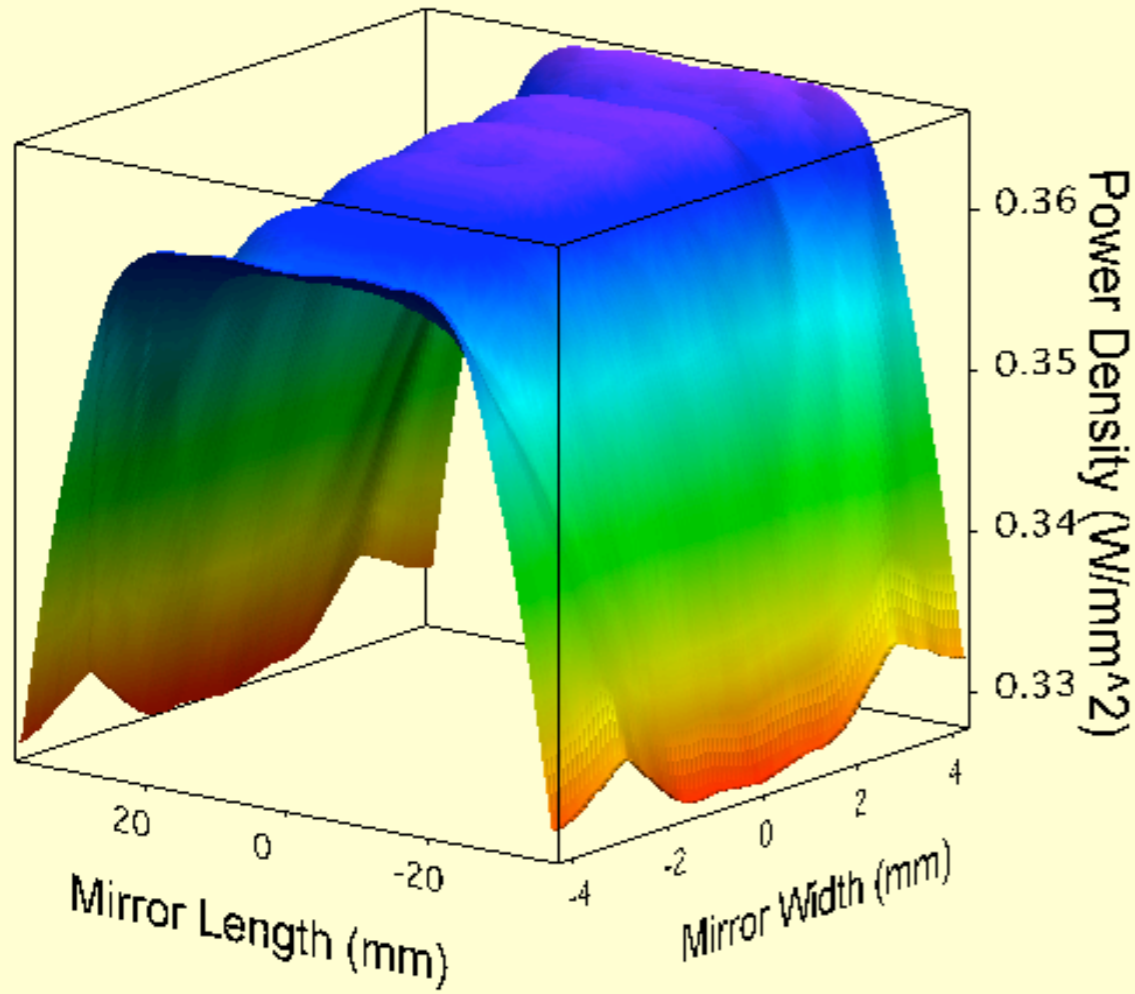


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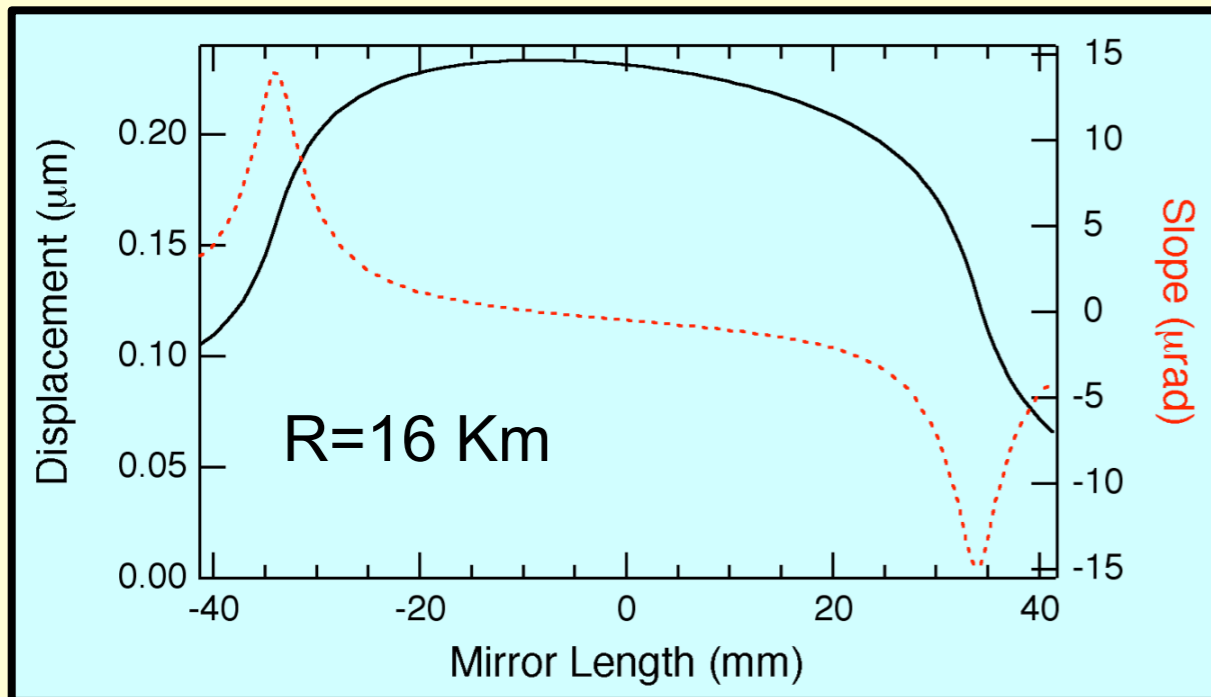
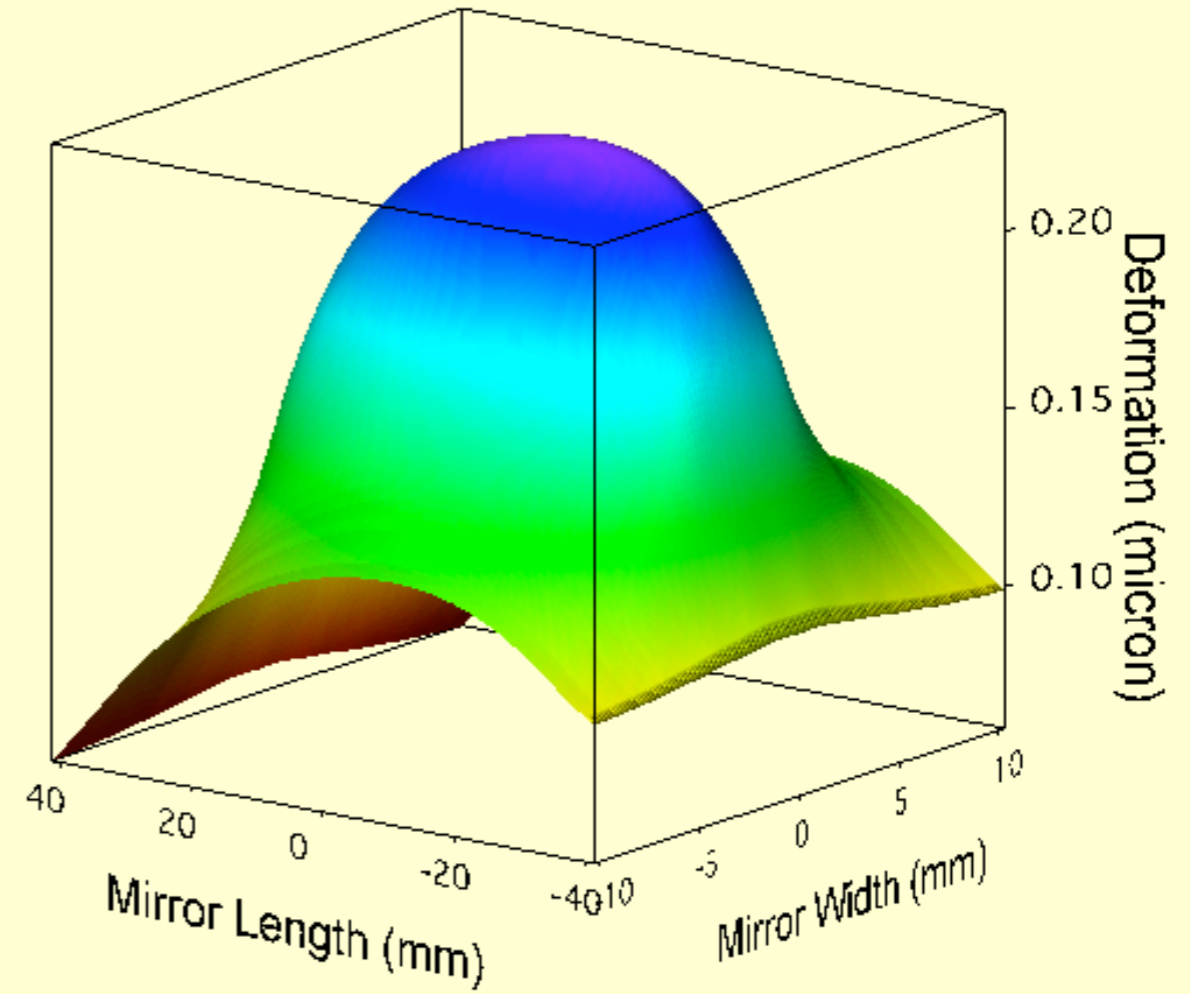


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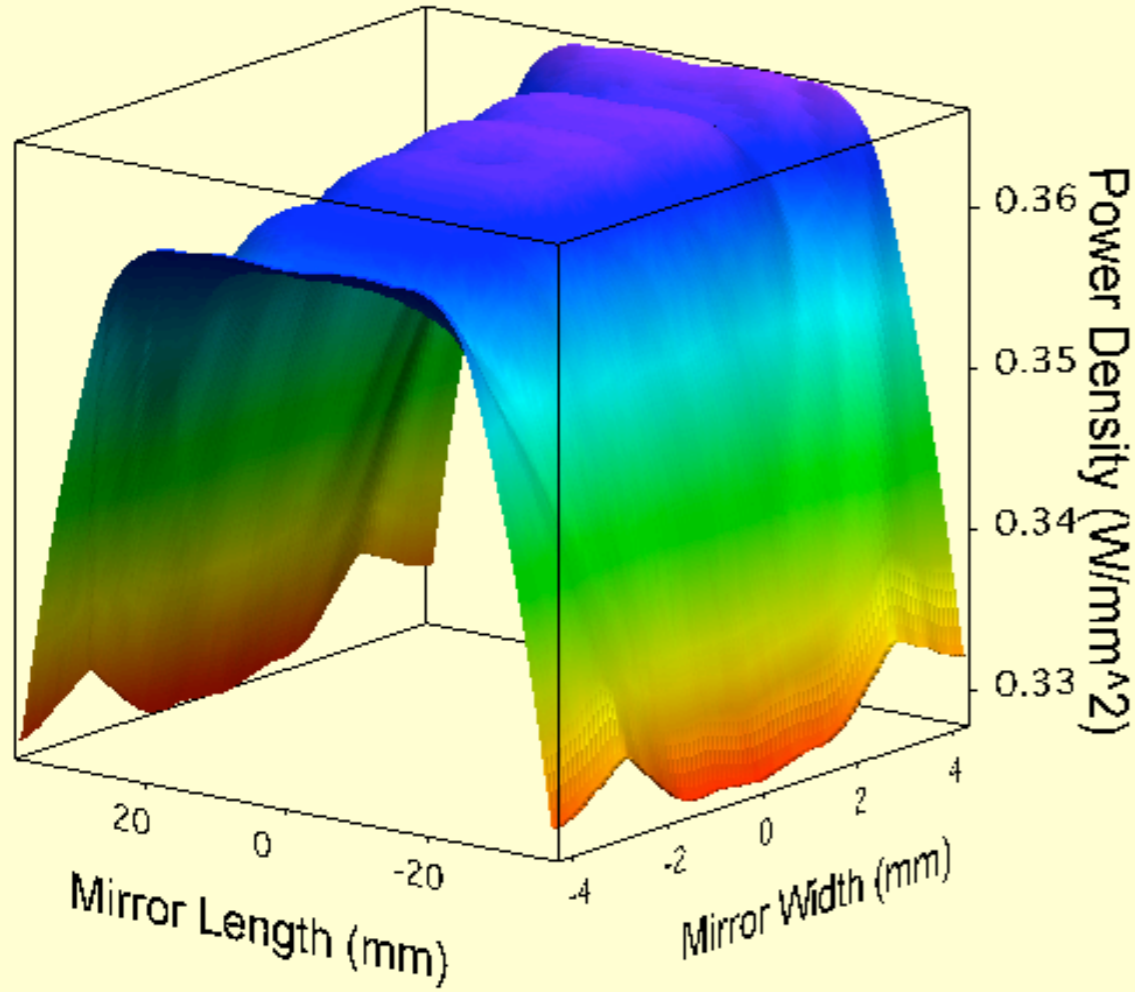


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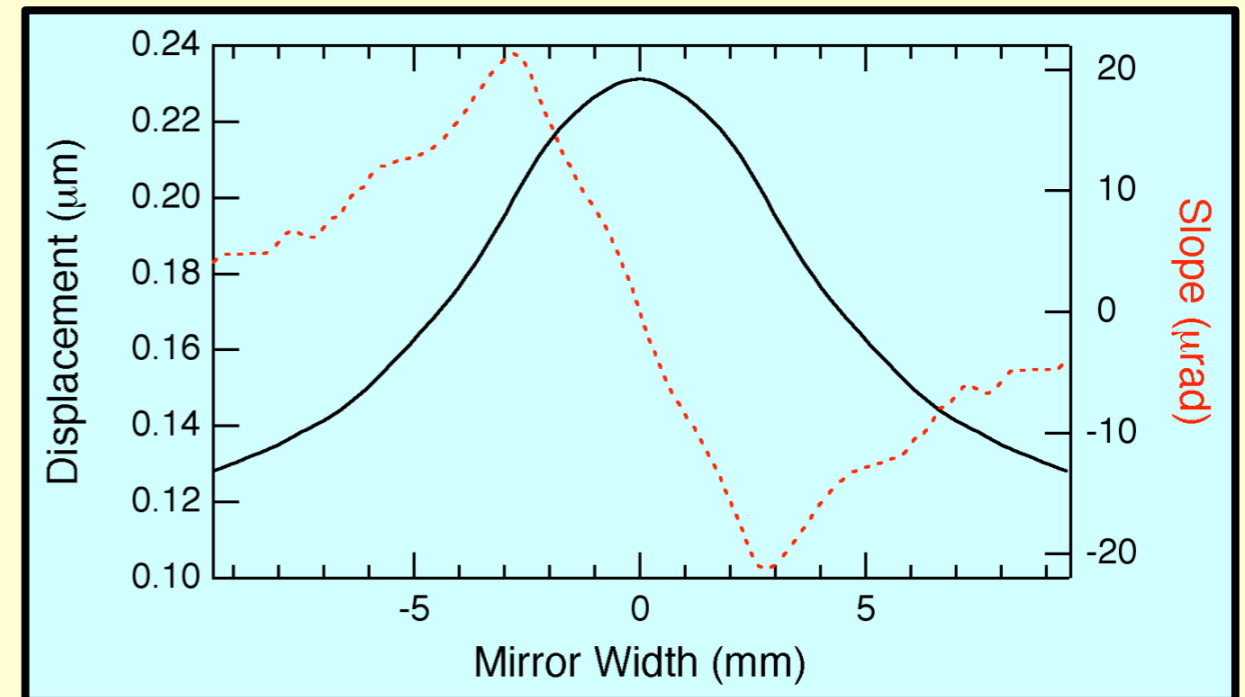
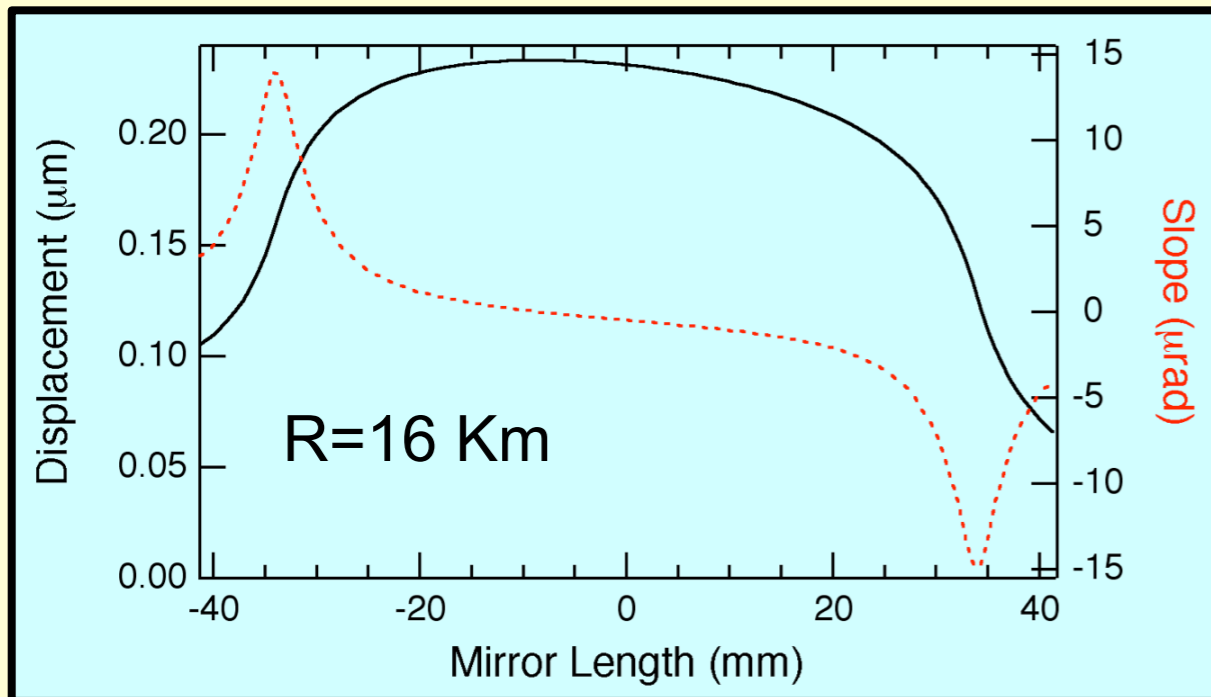
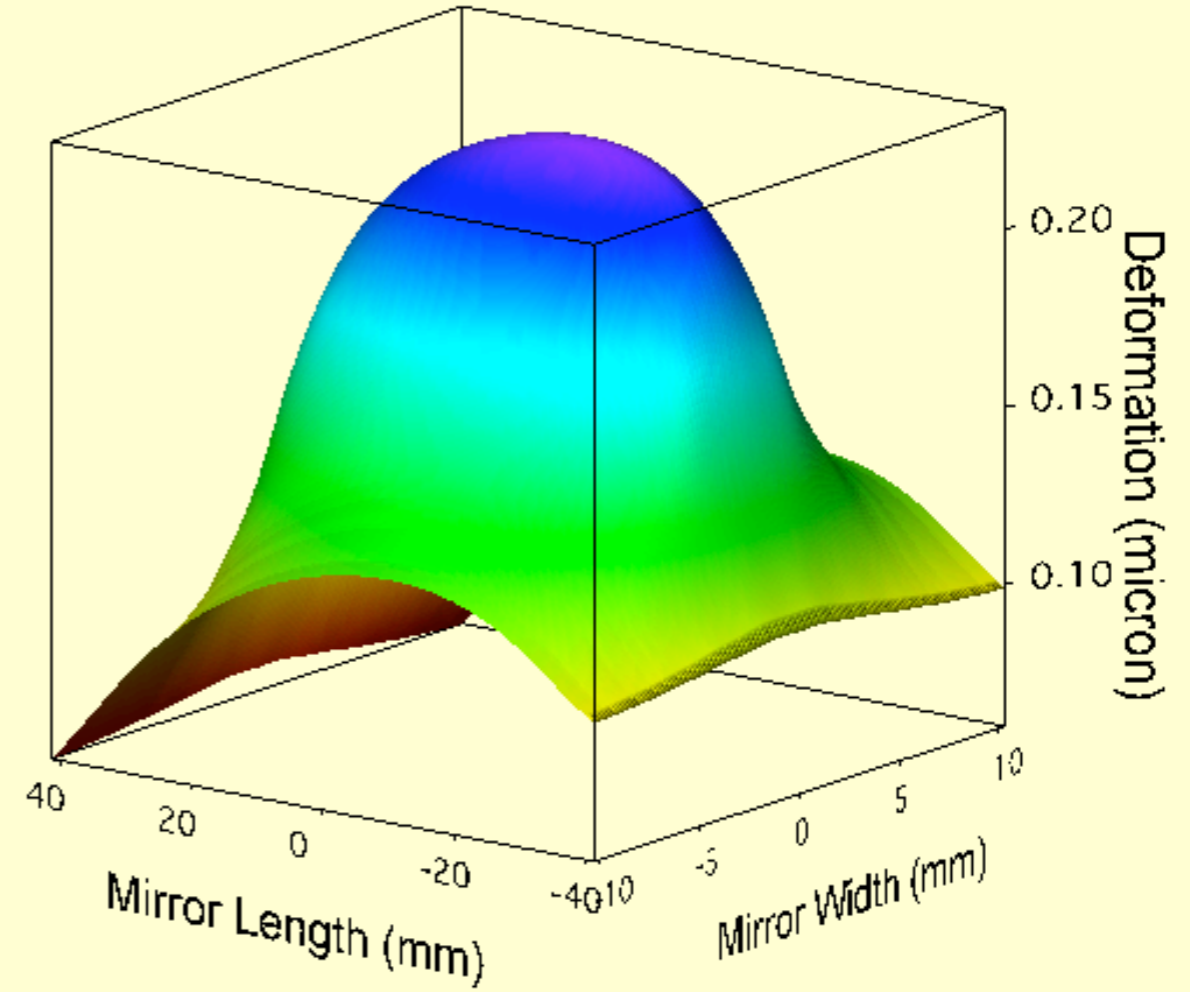


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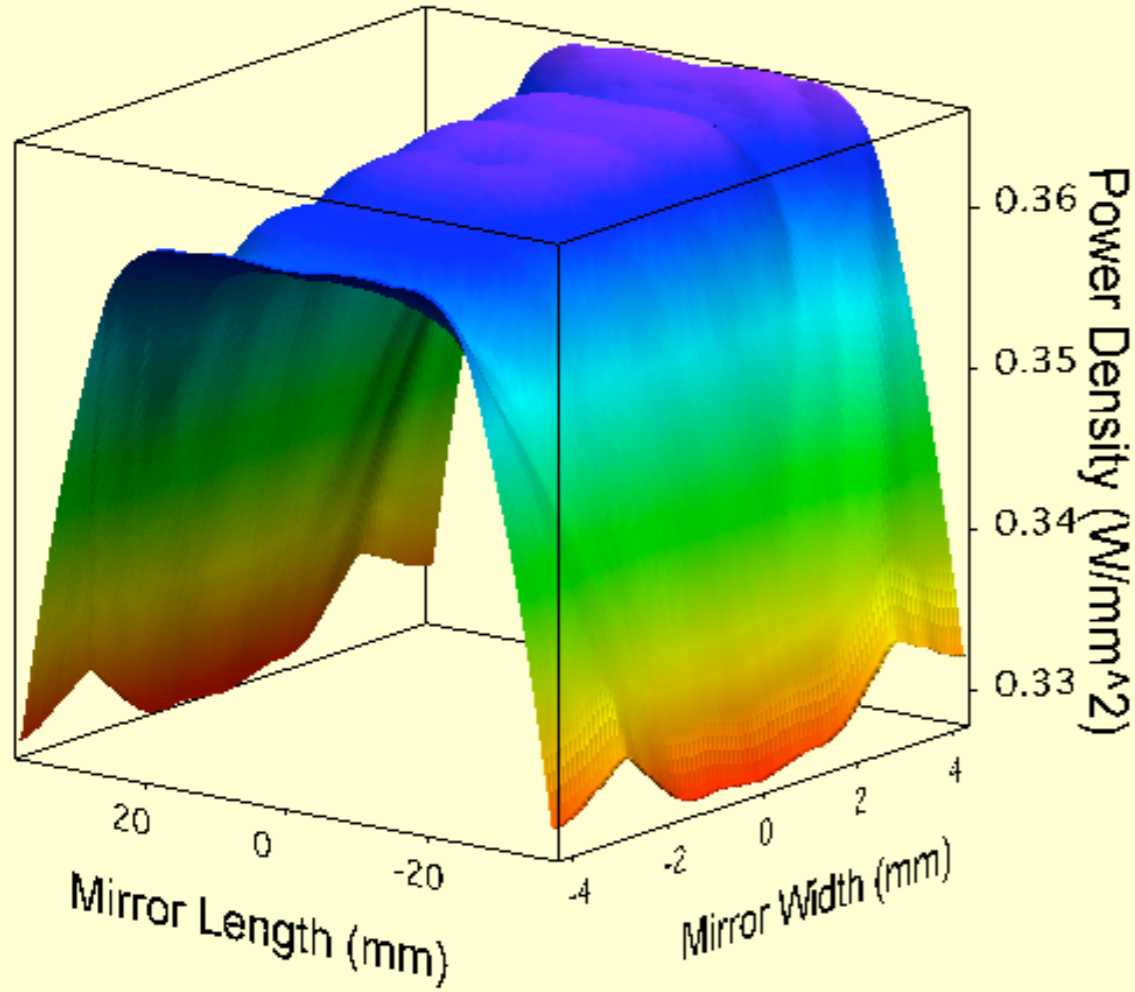


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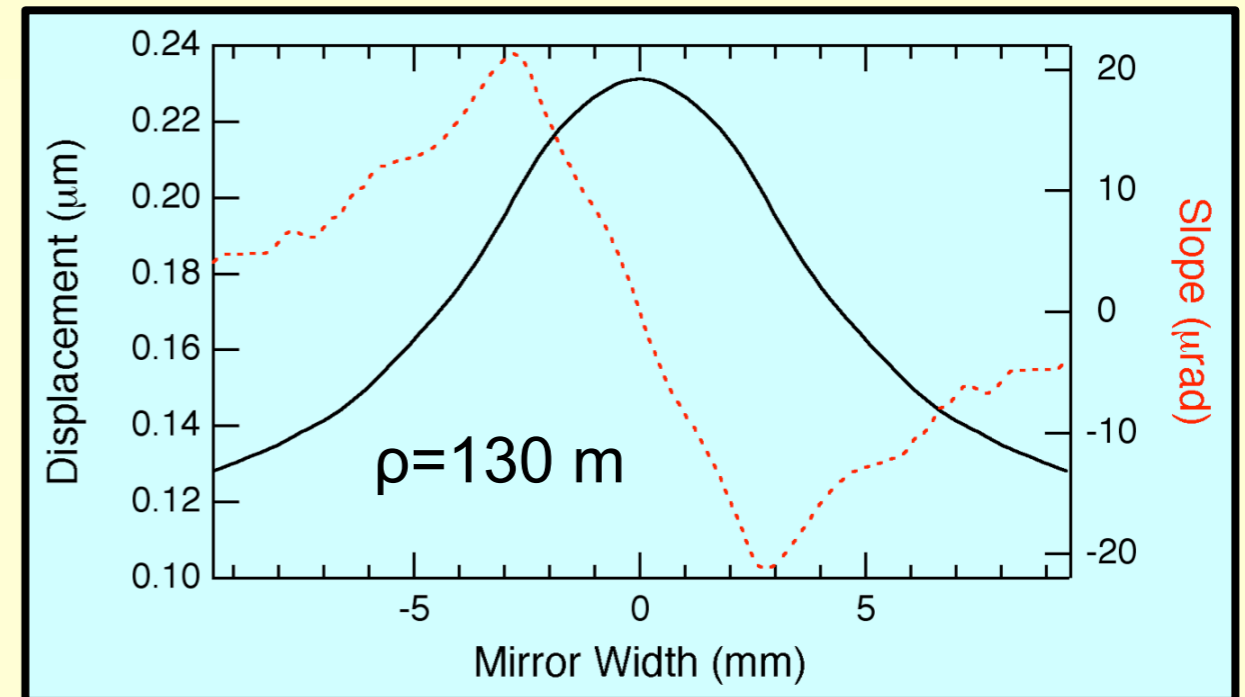
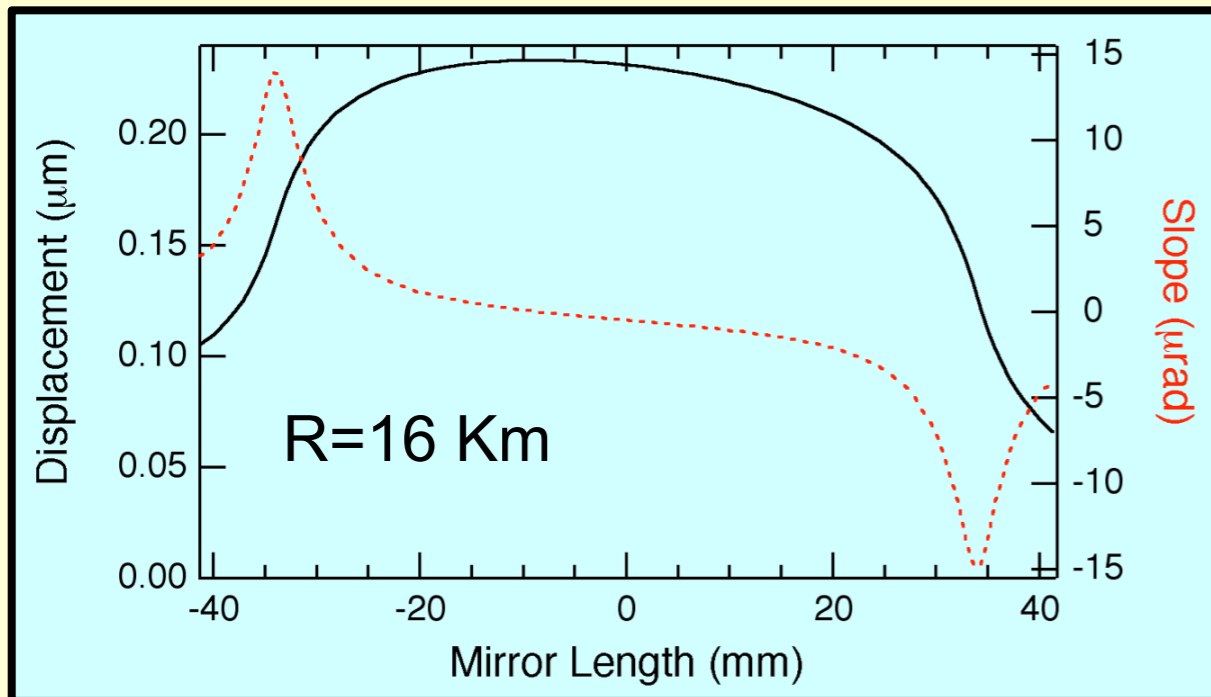
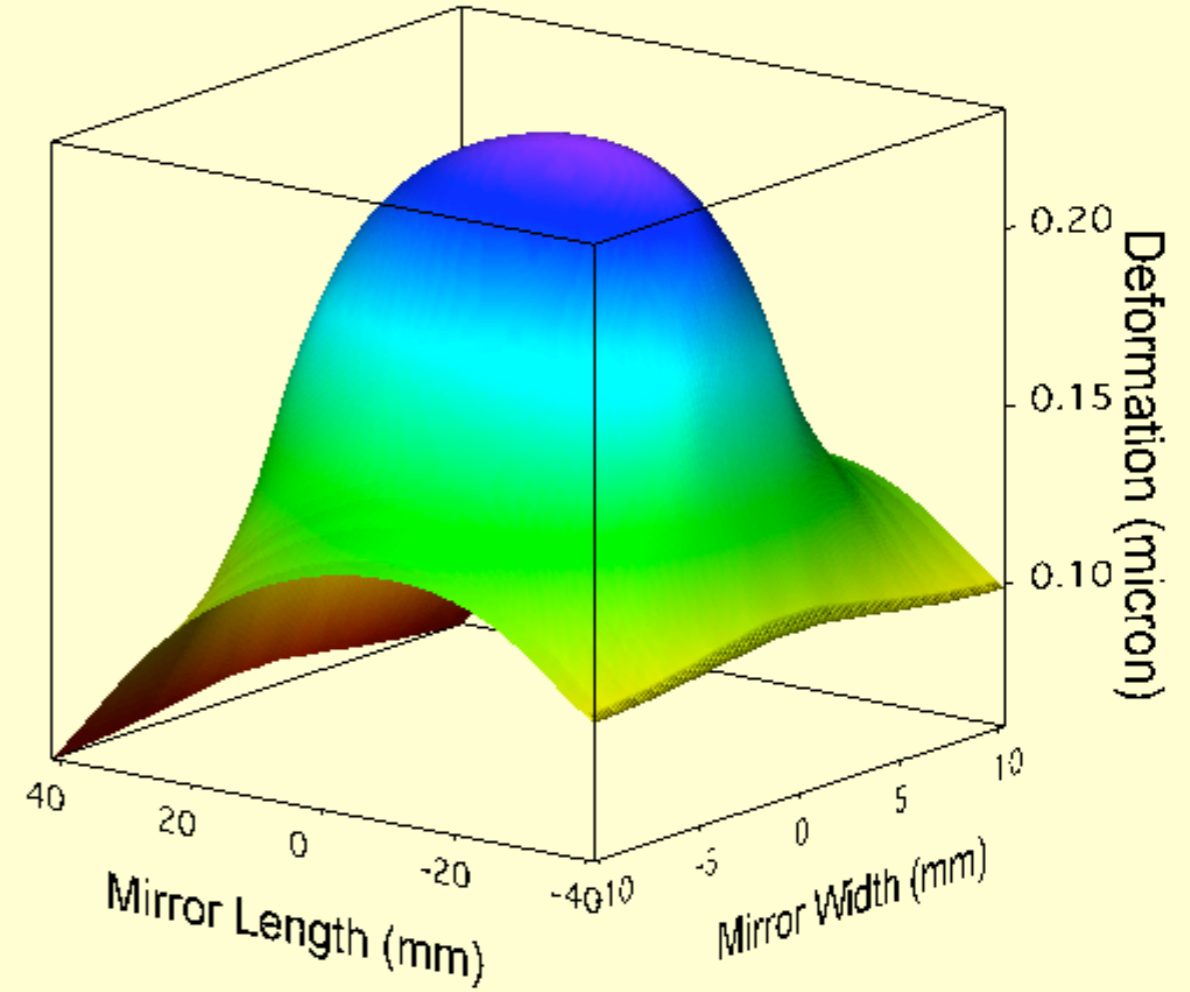


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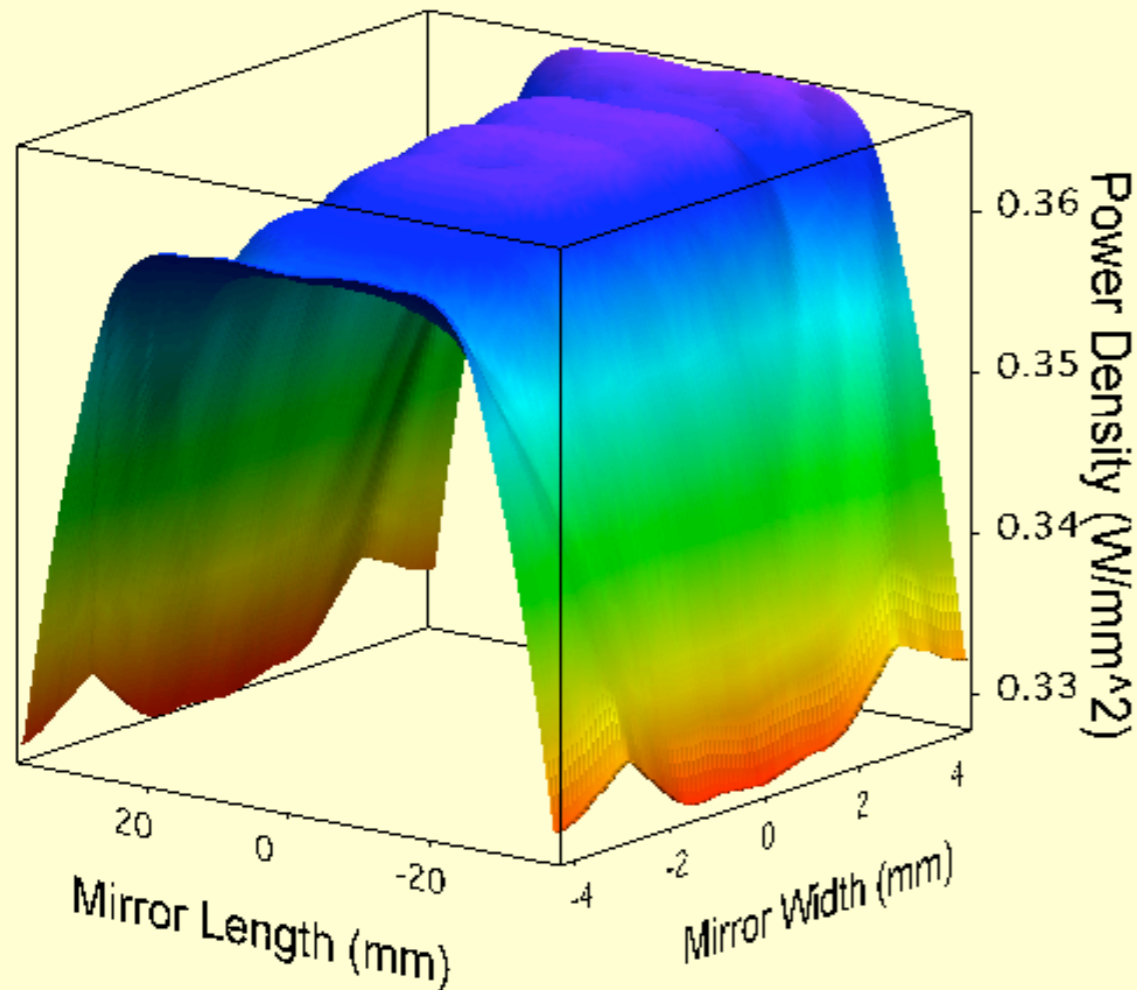


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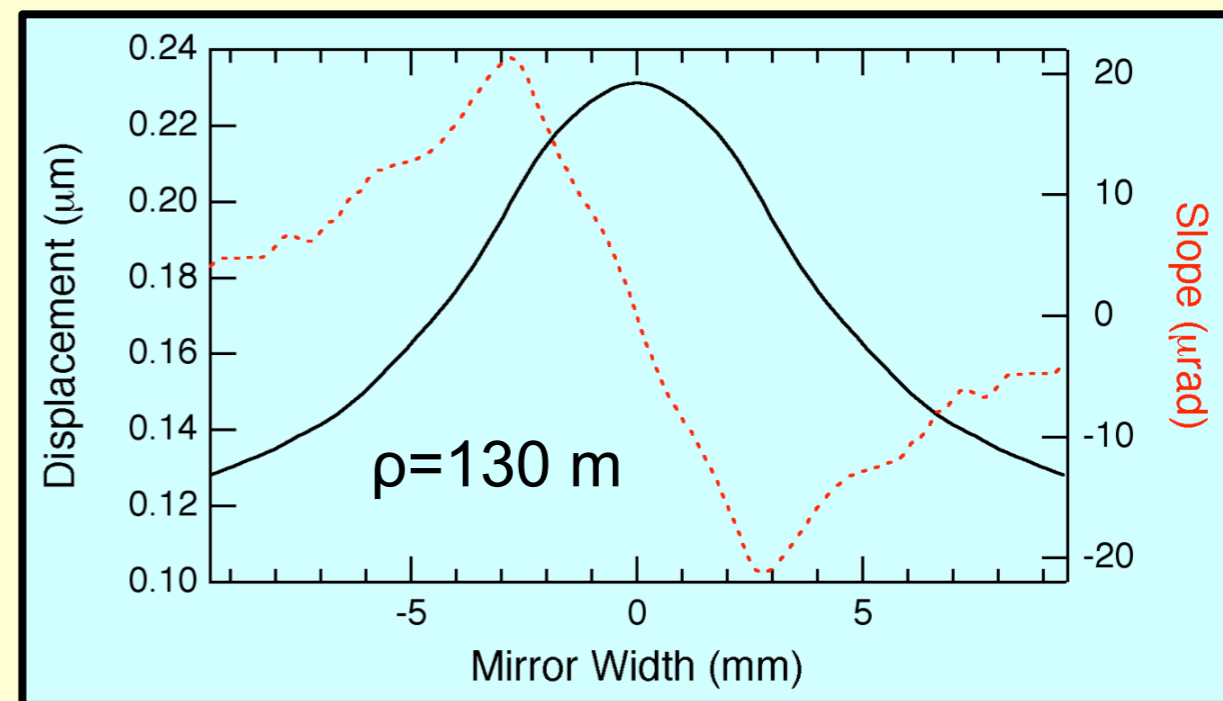
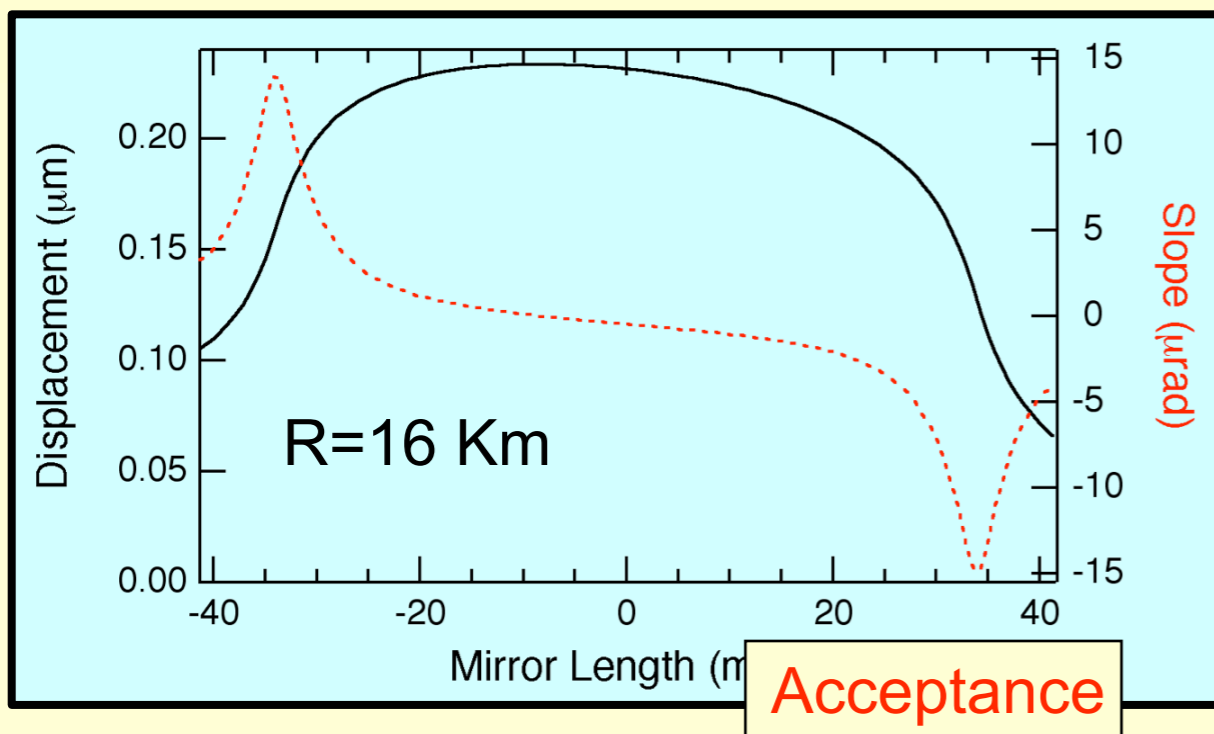
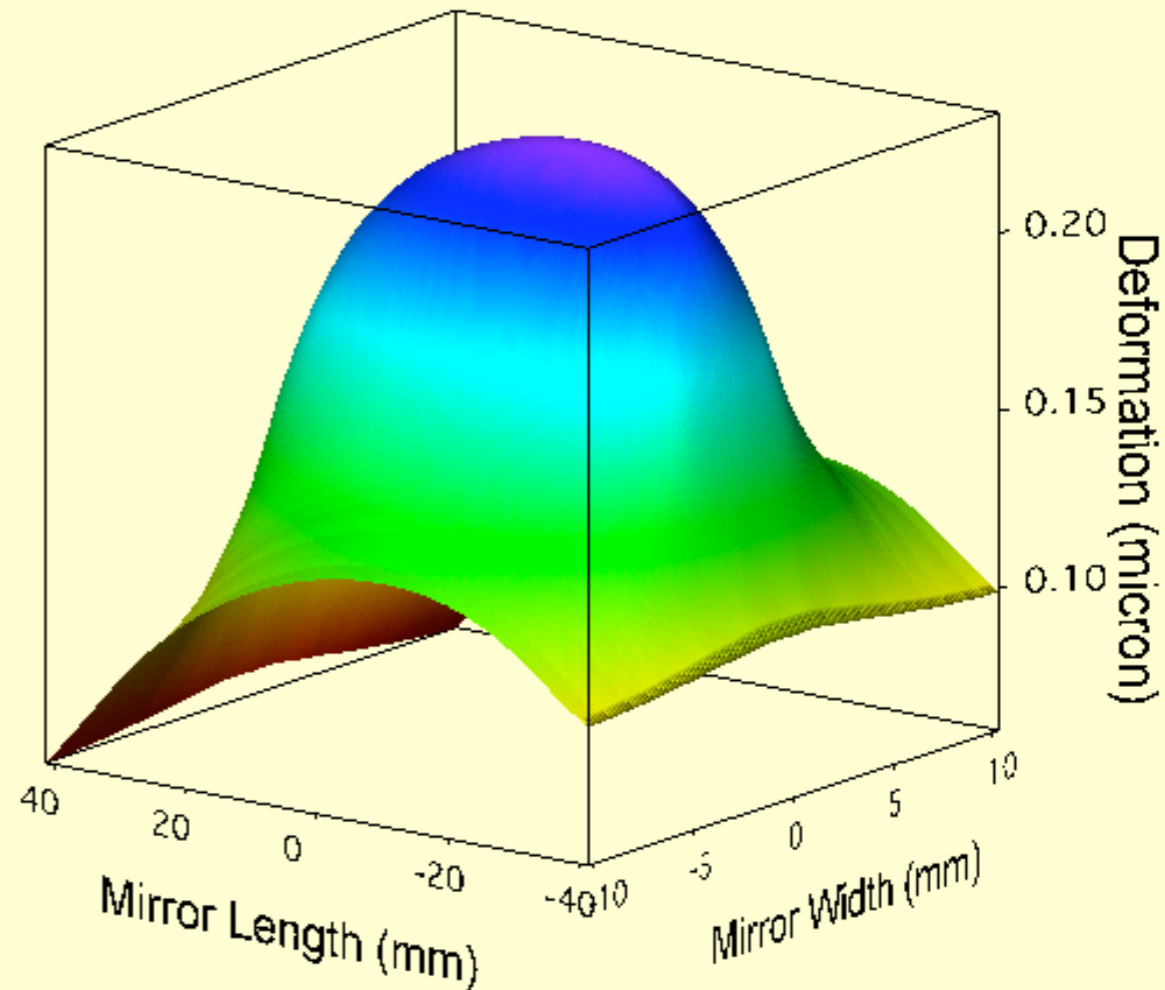


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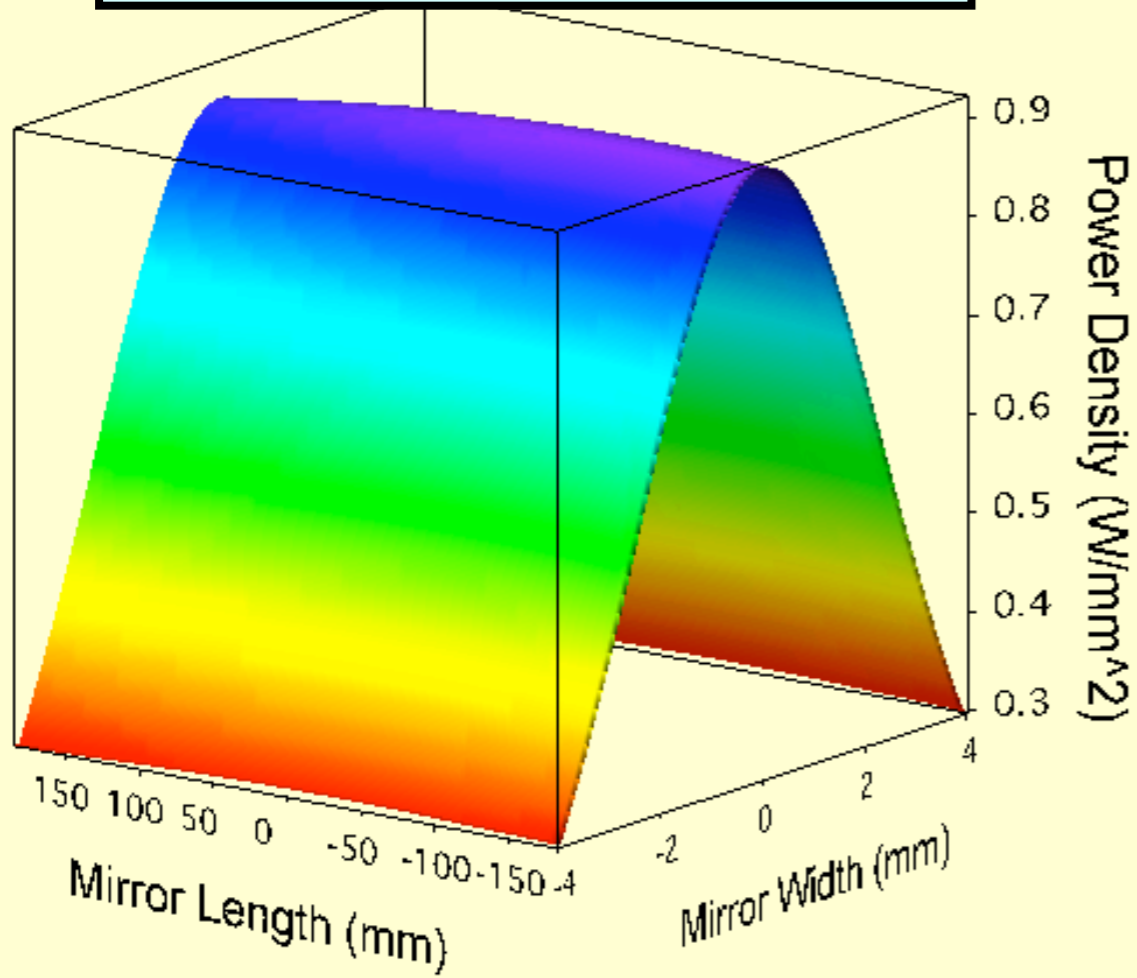


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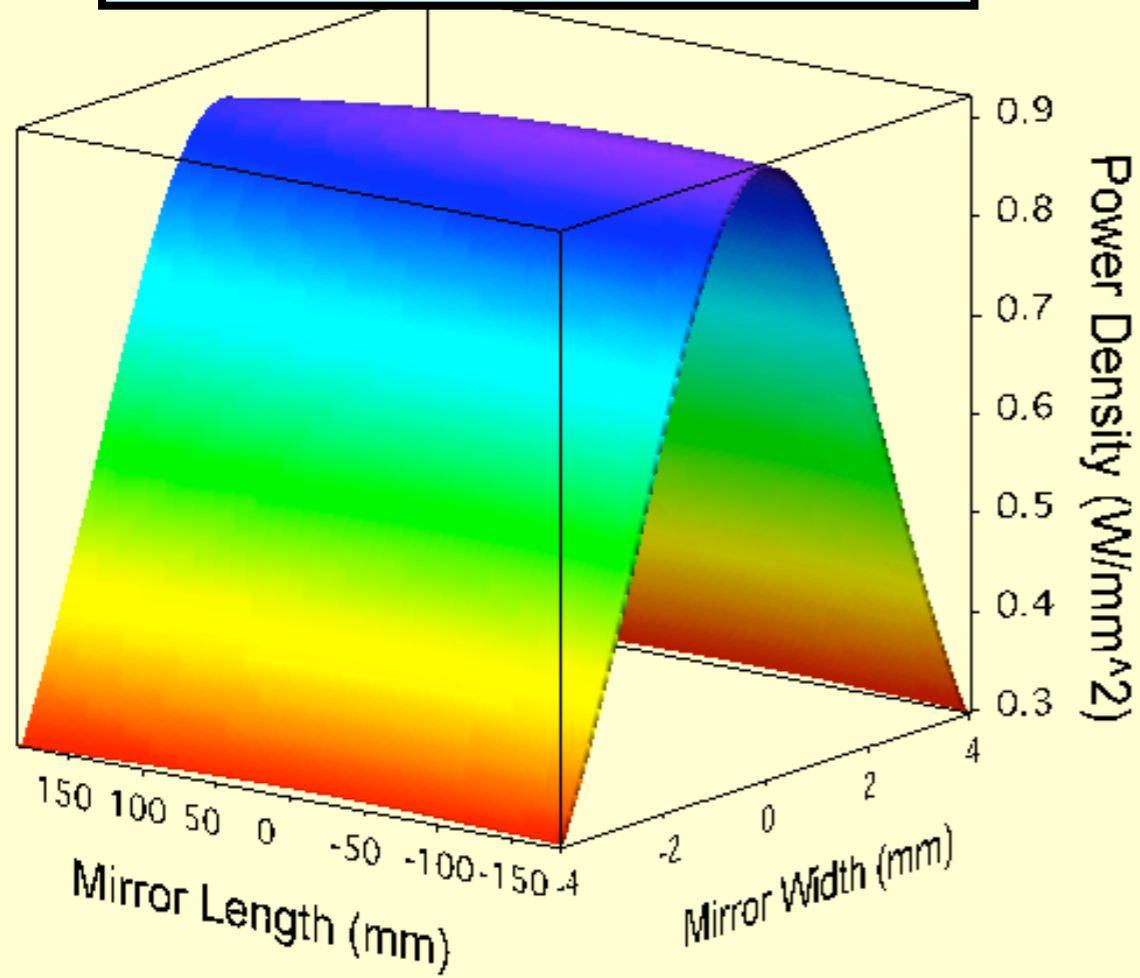
Power on M1

➔ Total absorbed 1.9 kW

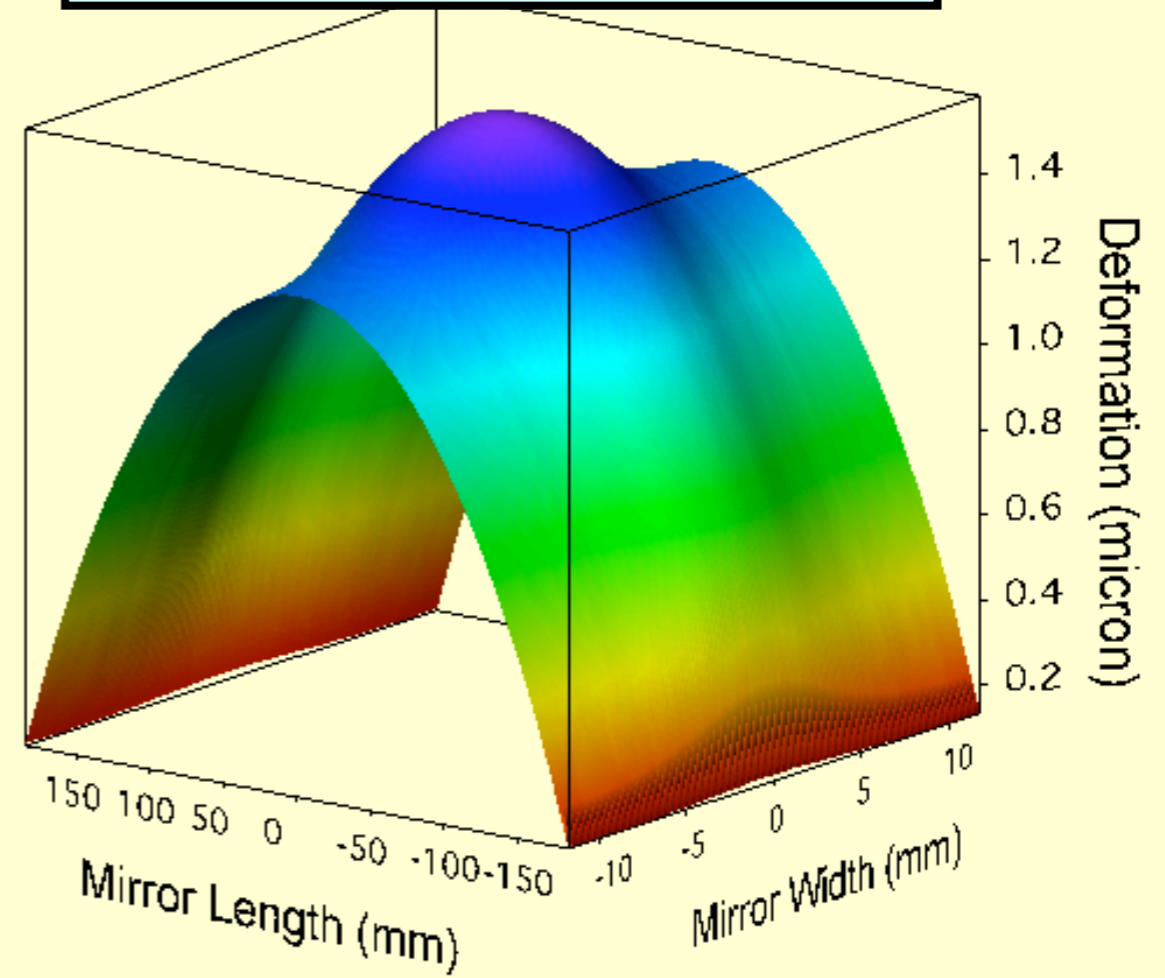


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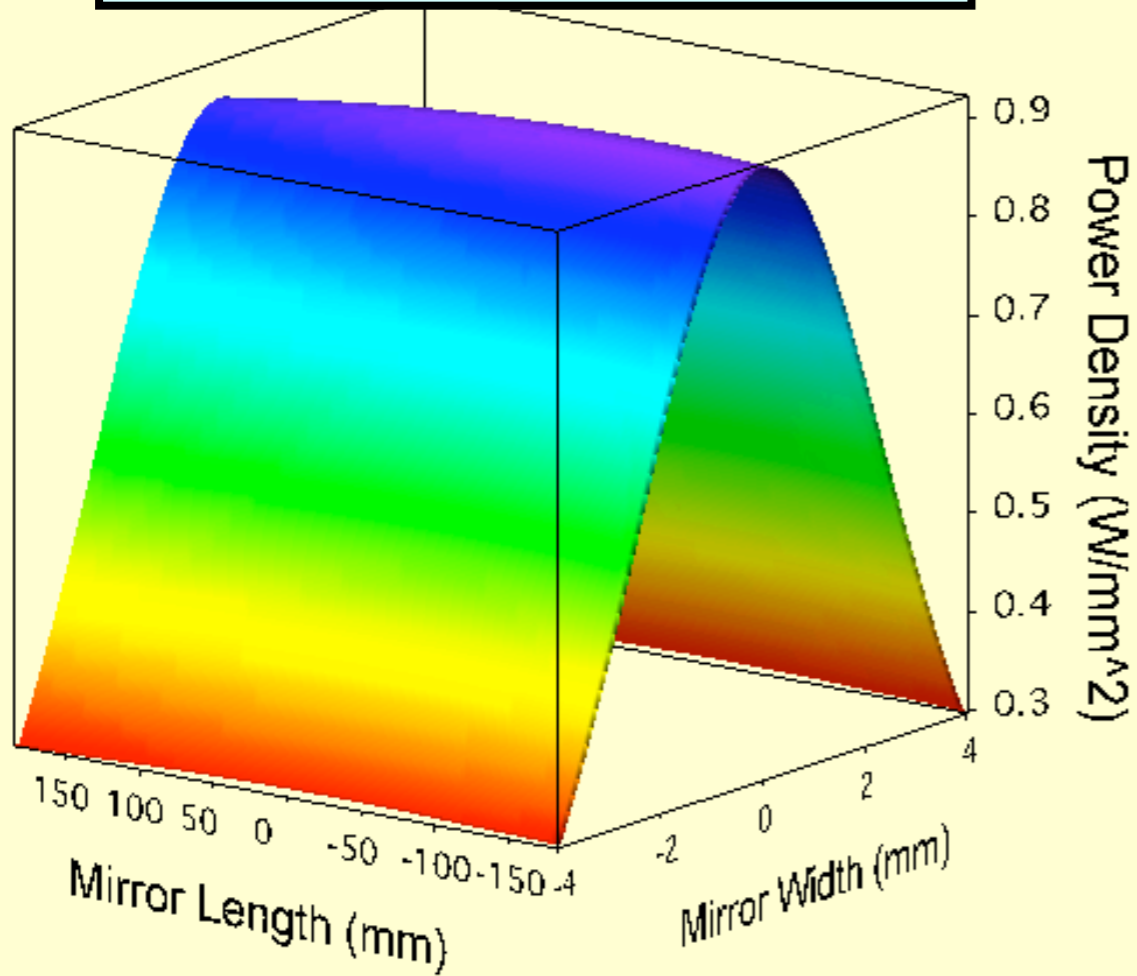


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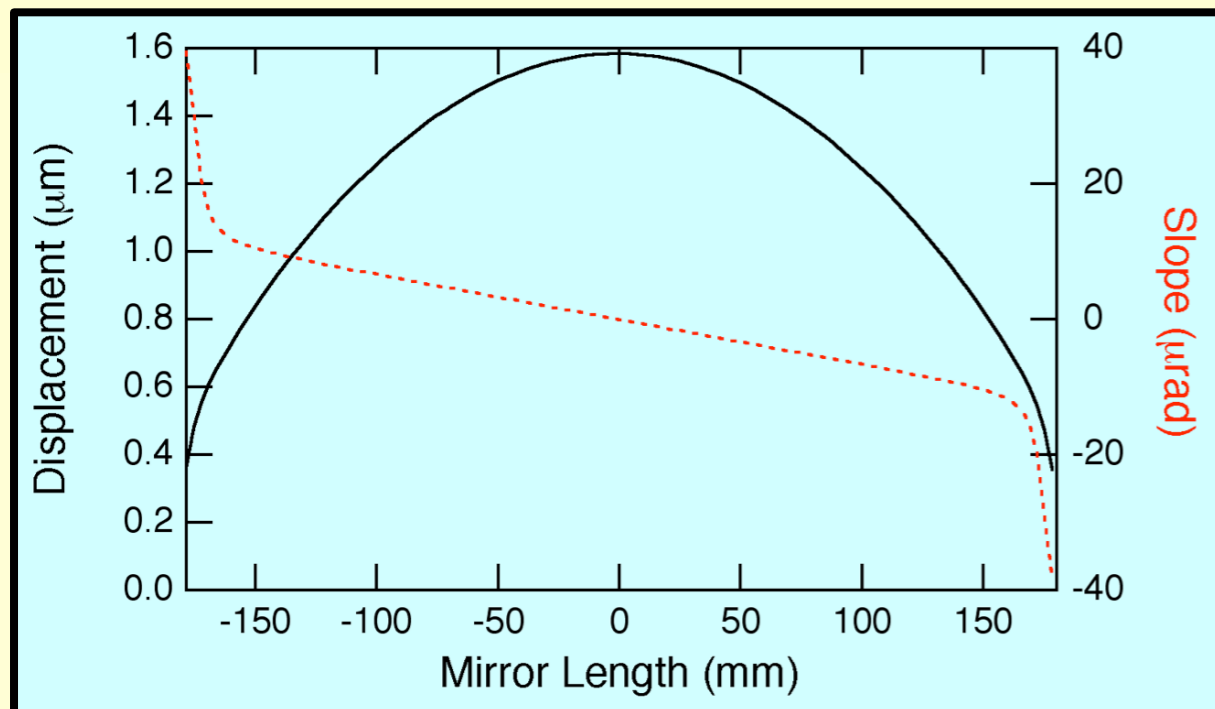
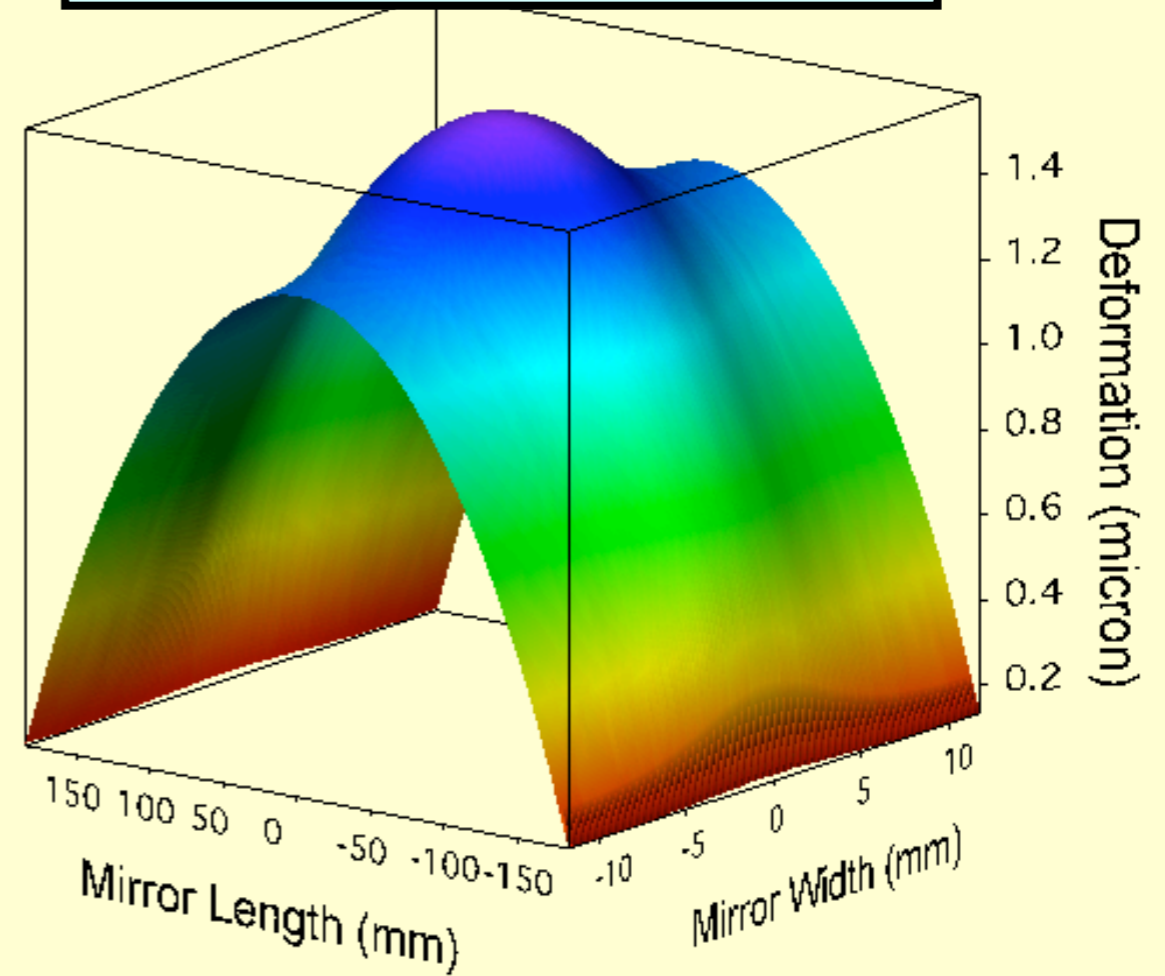


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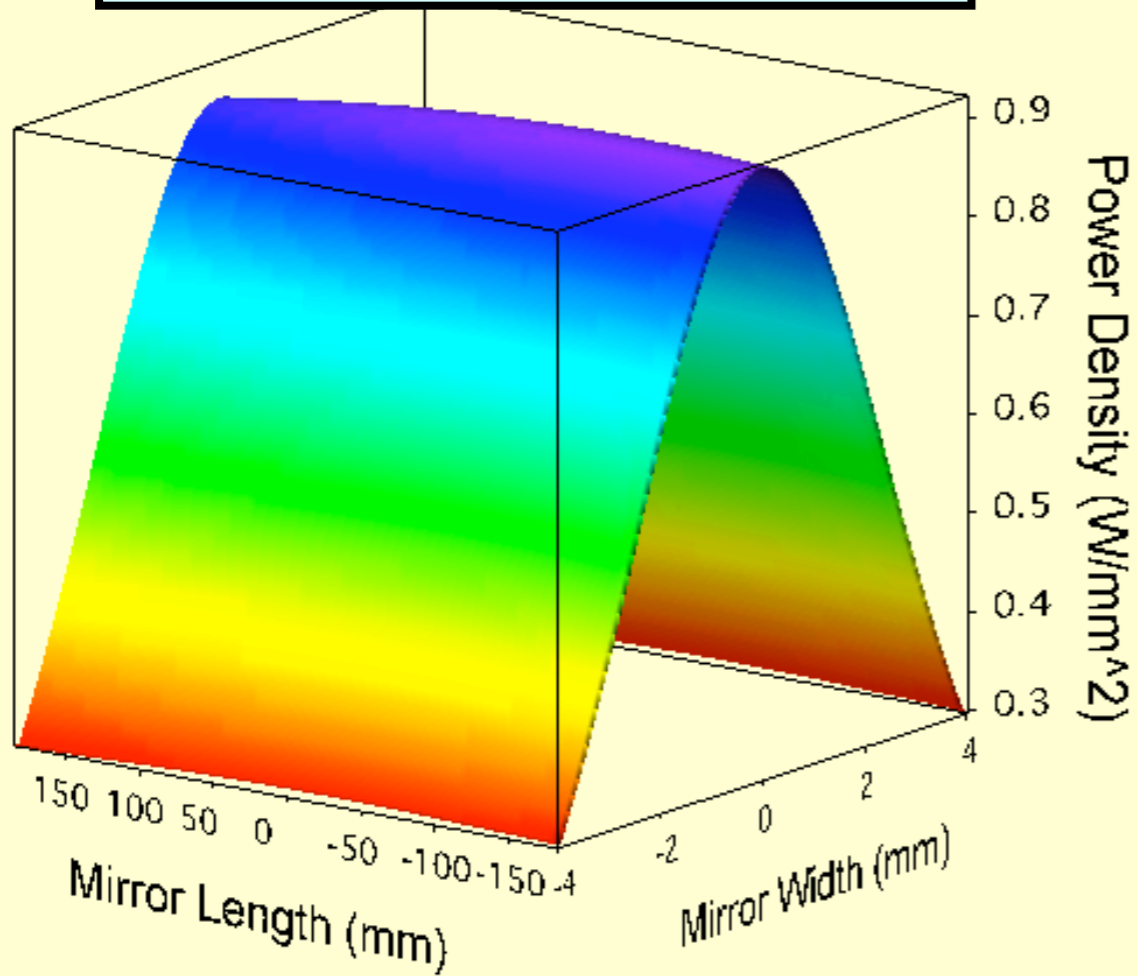


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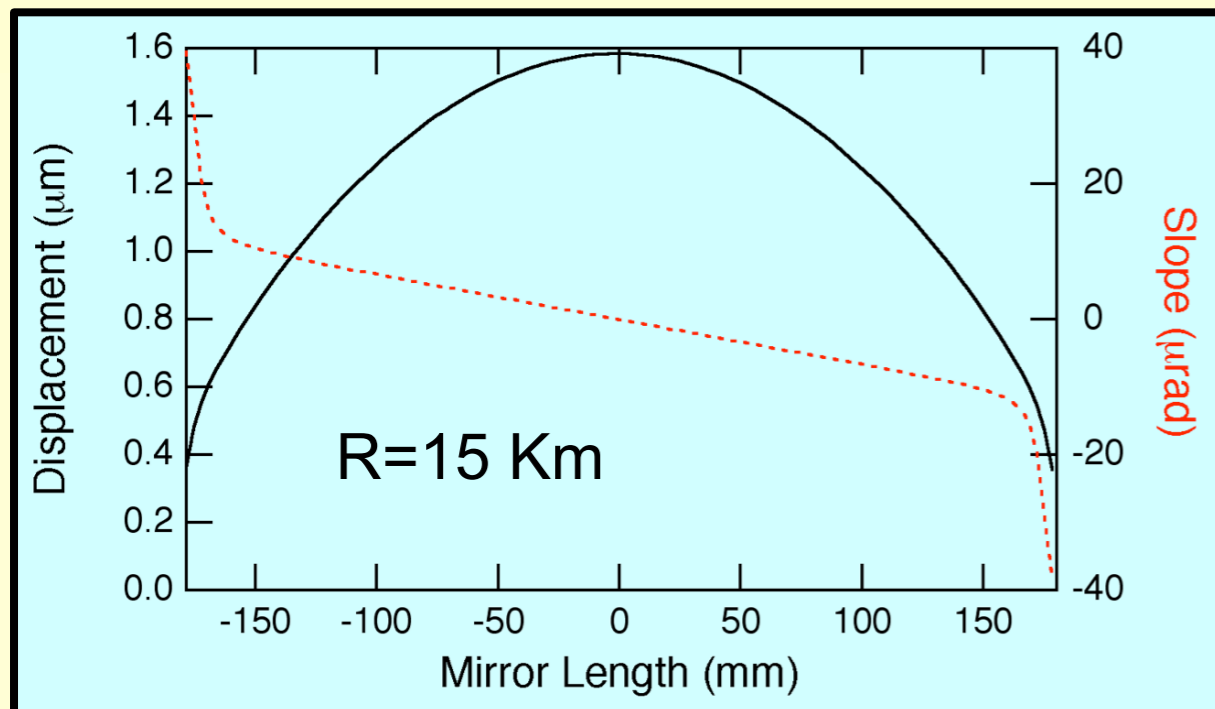
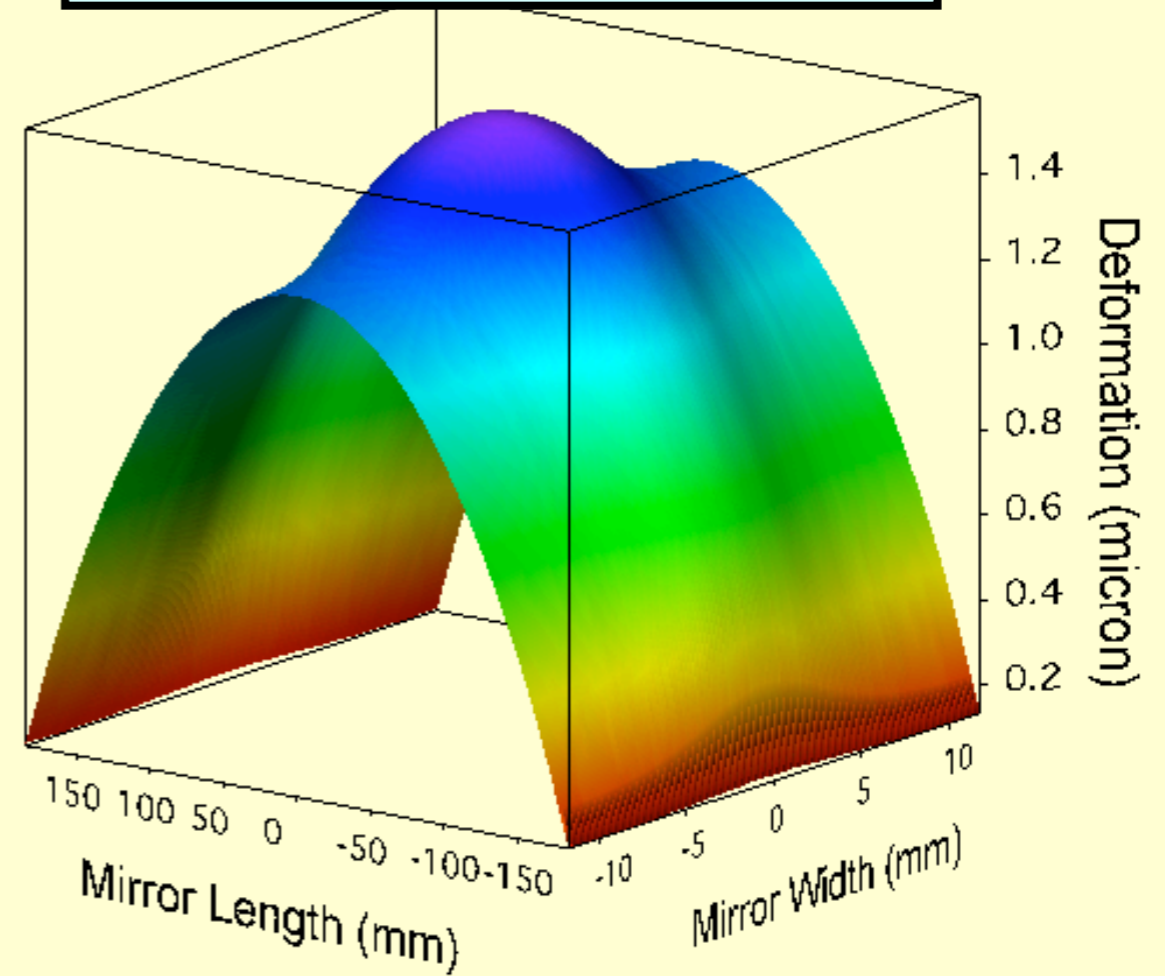


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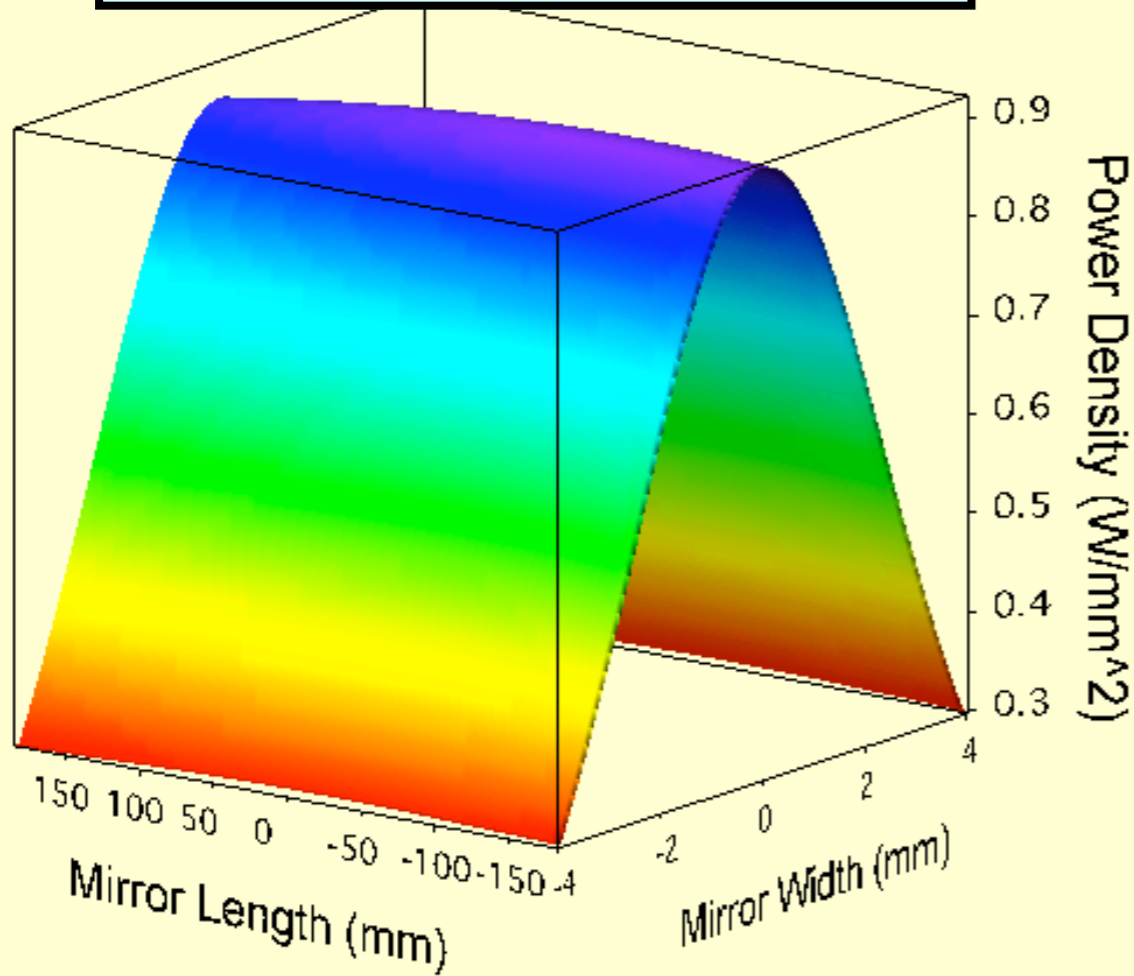


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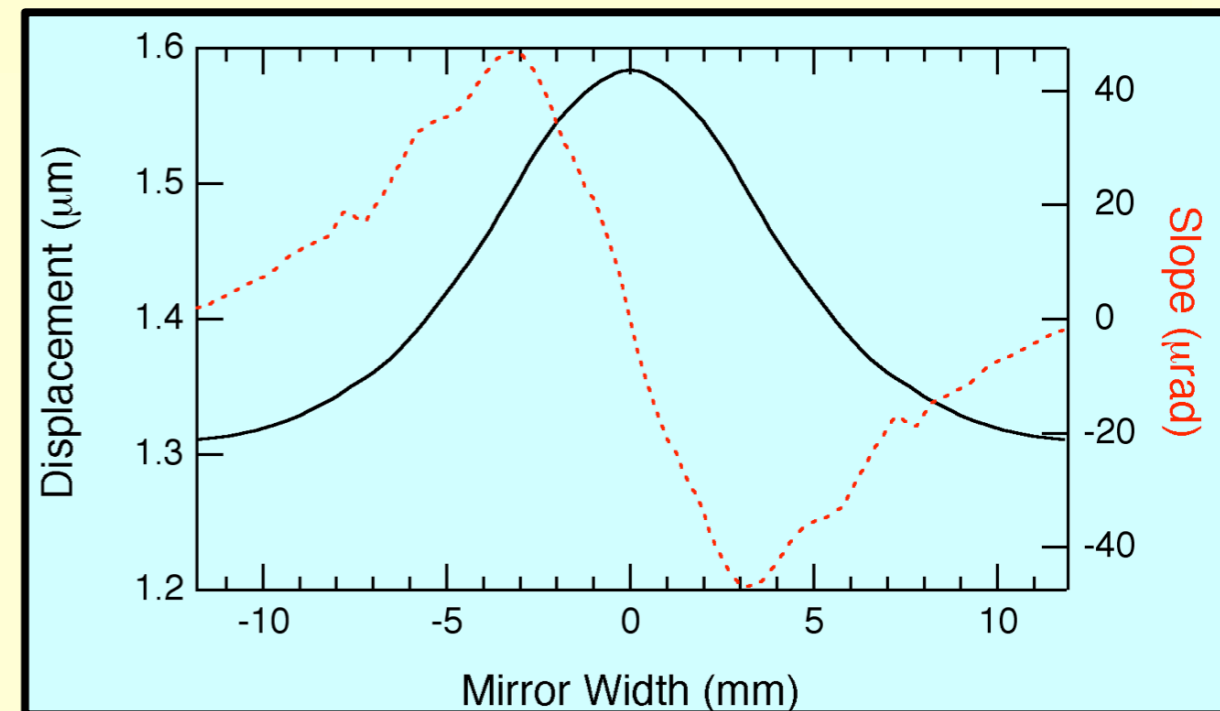
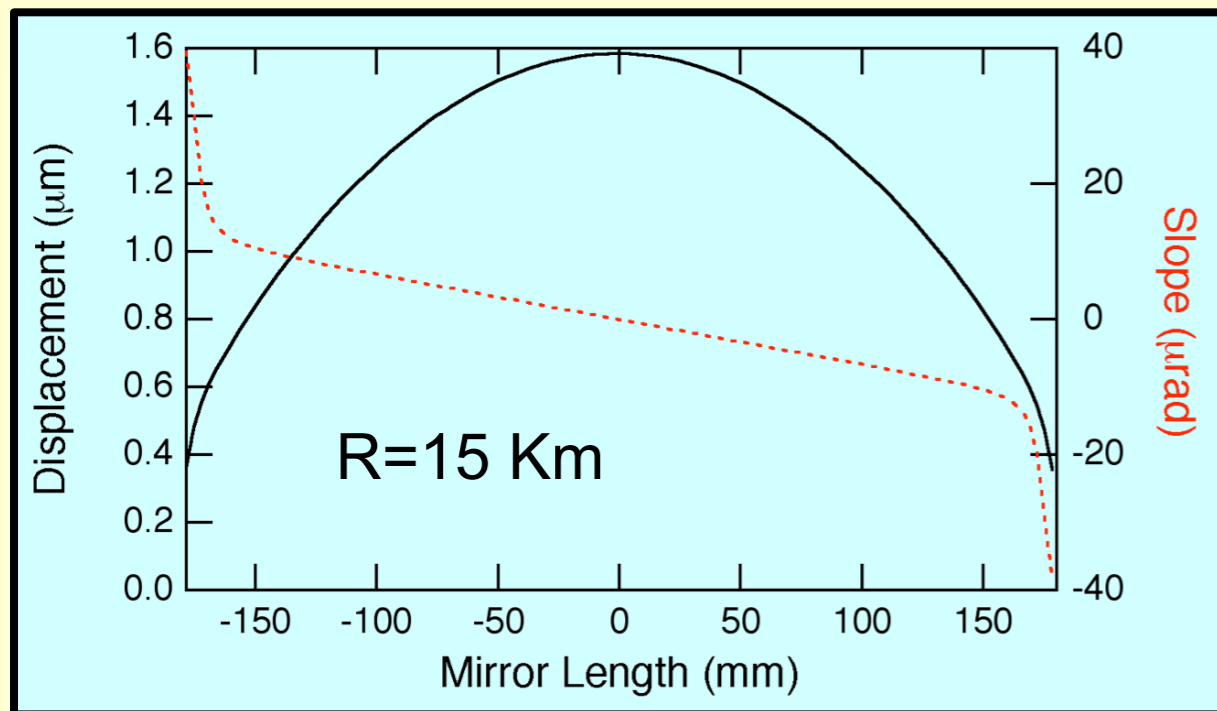
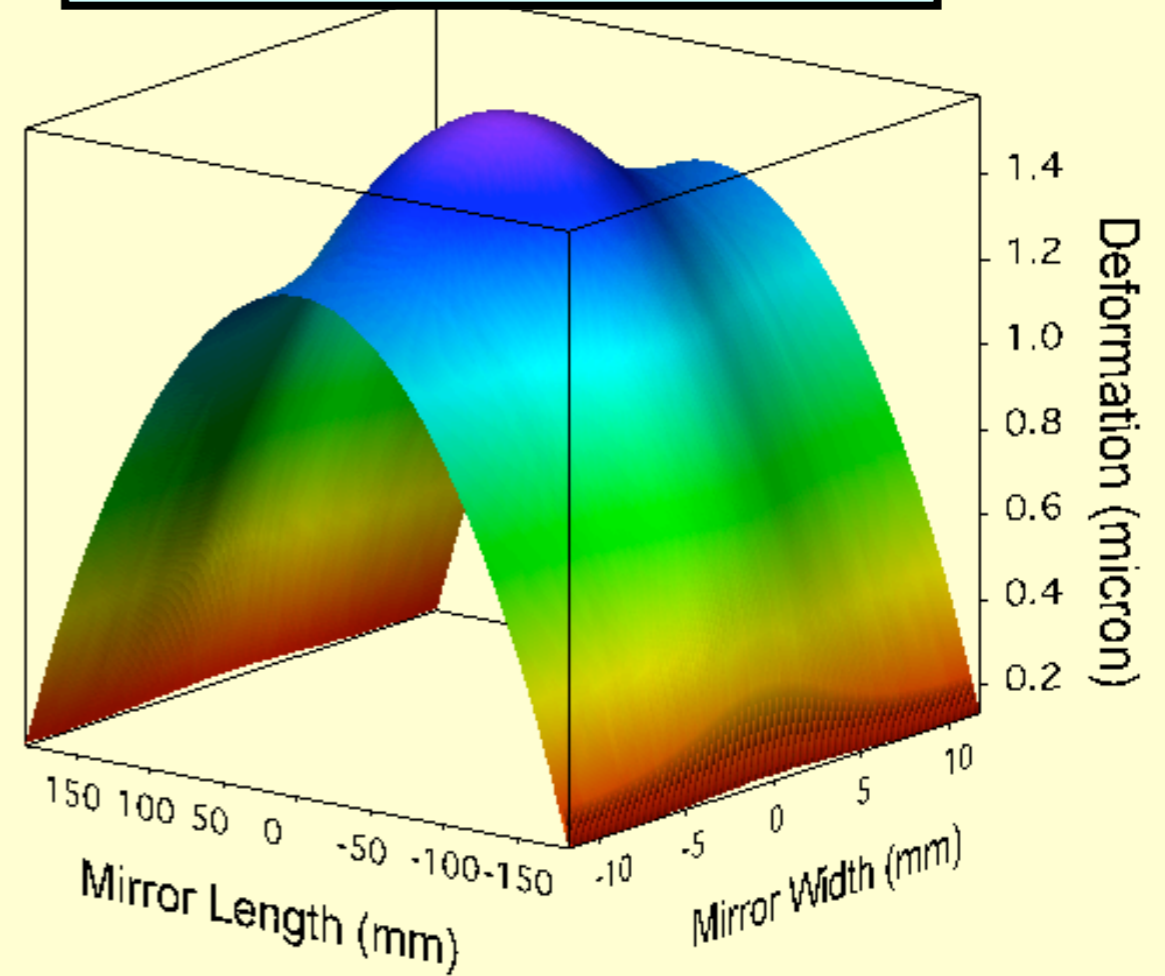


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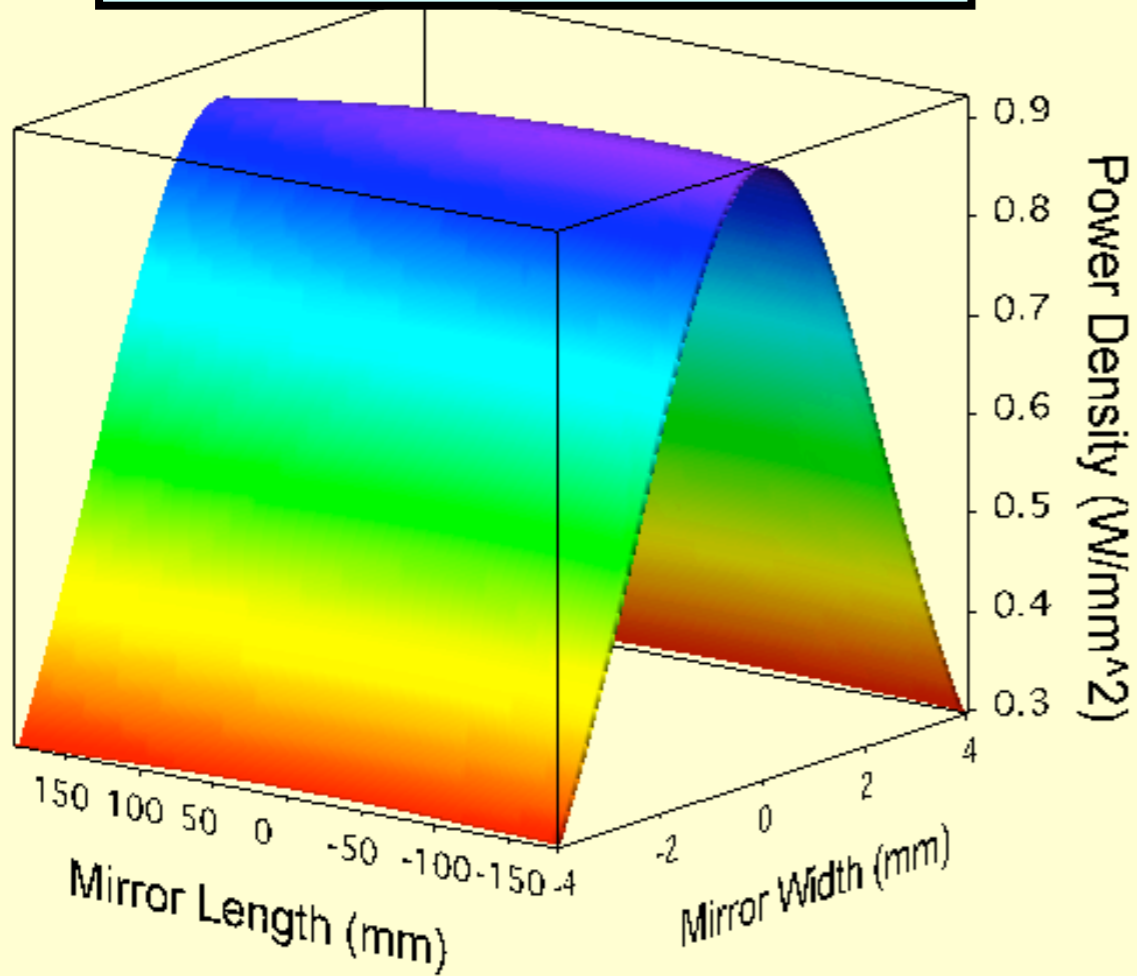


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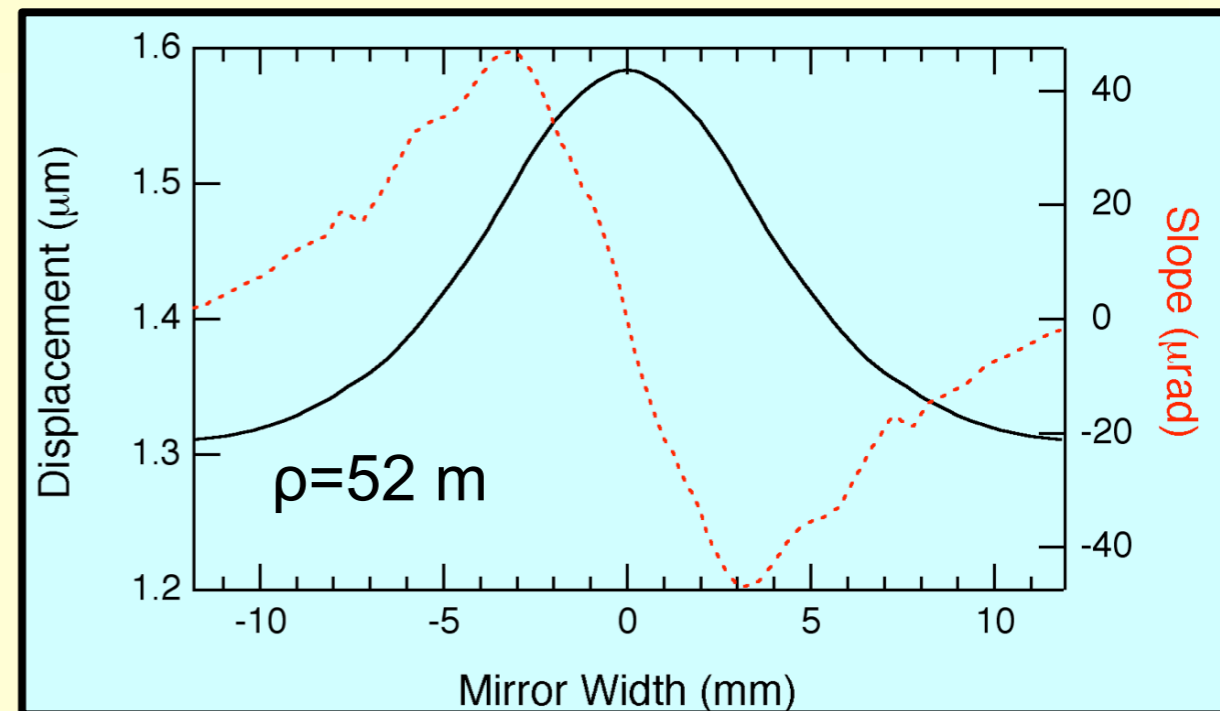
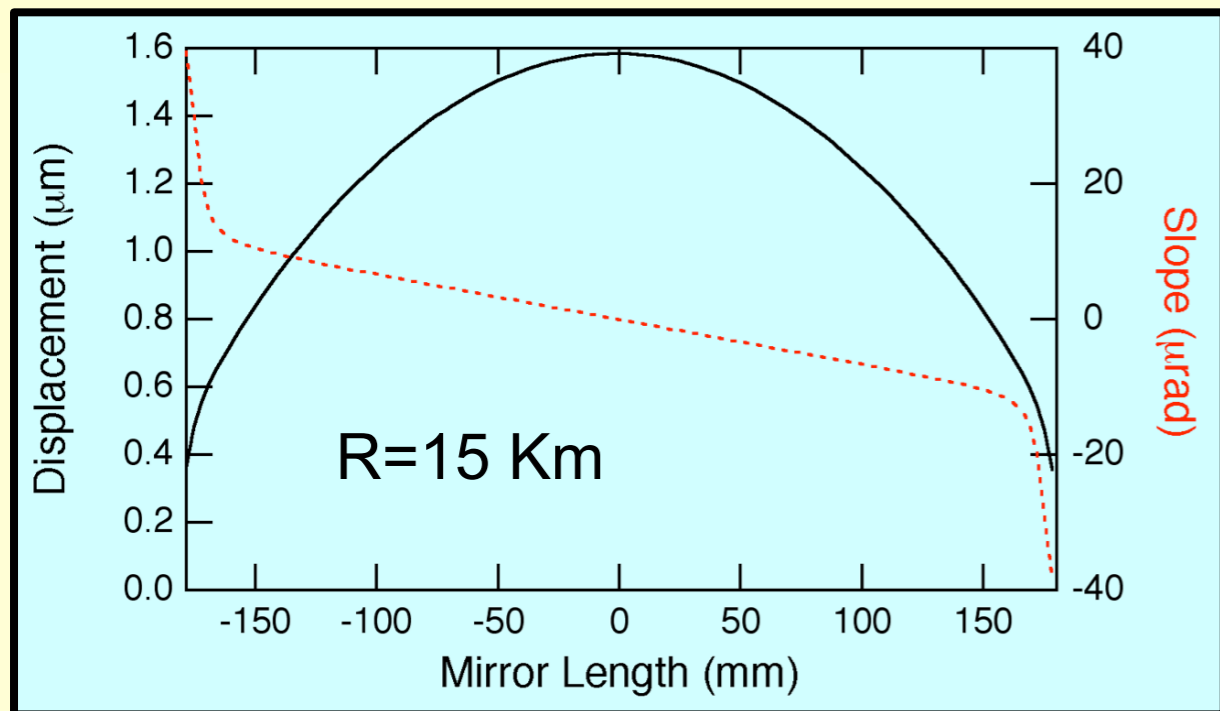
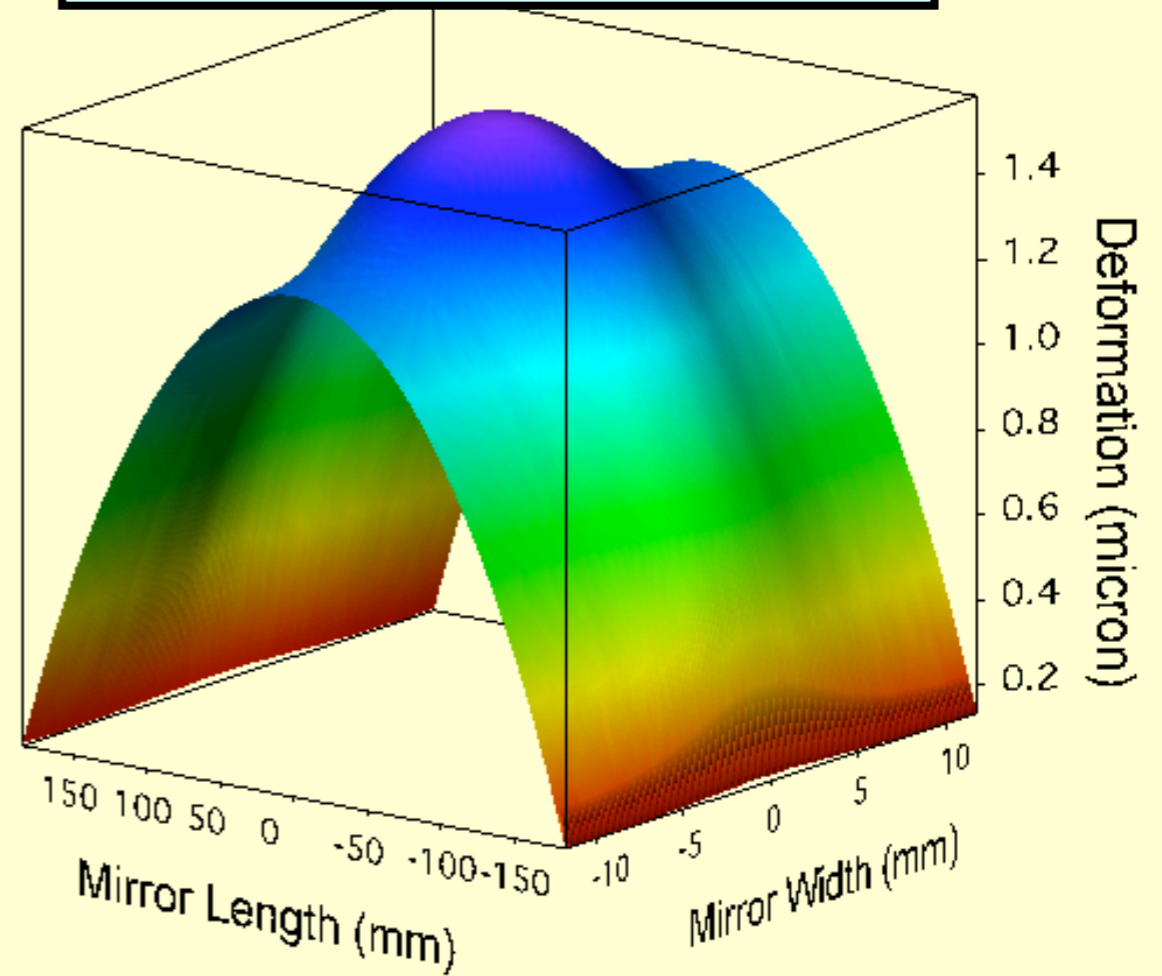


Power on M1

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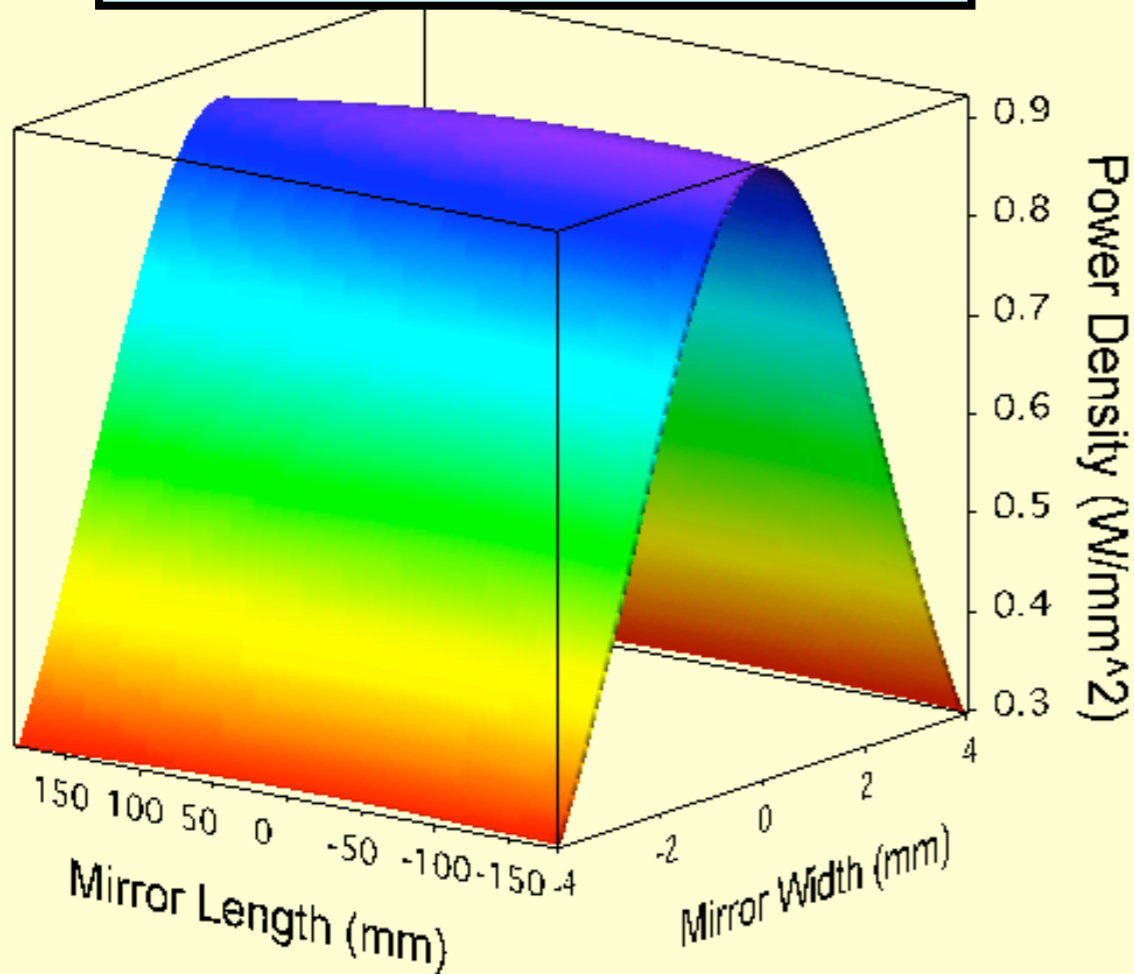


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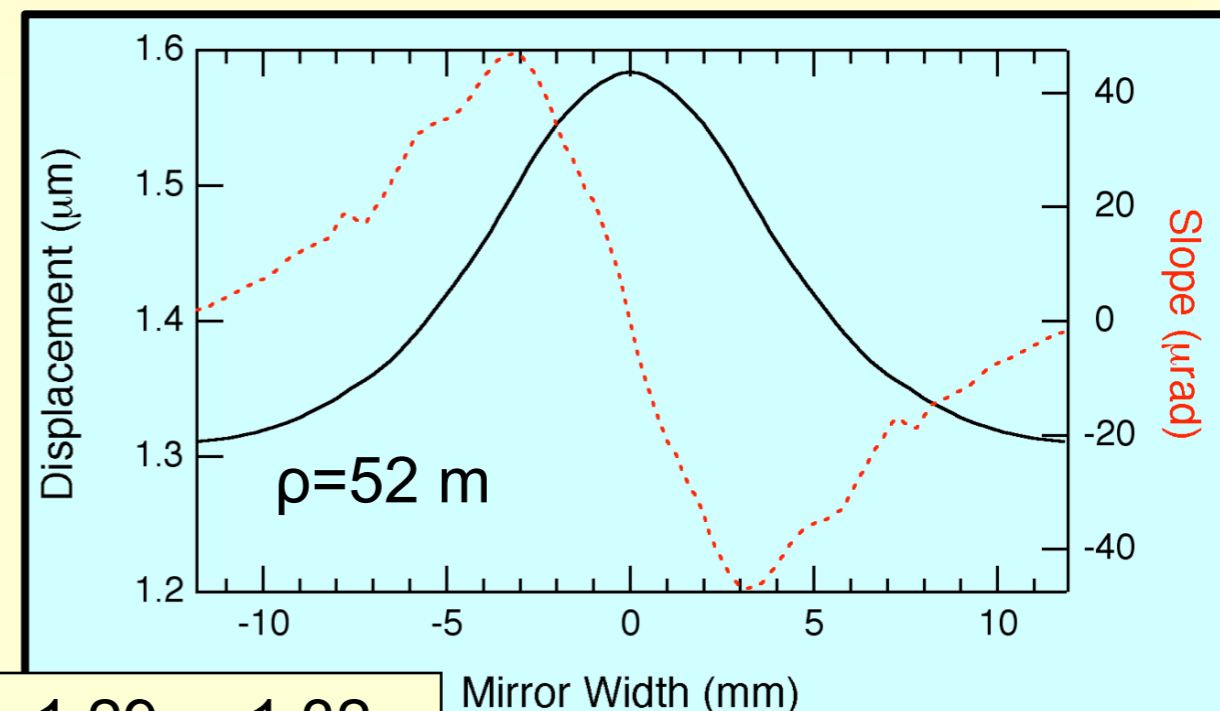
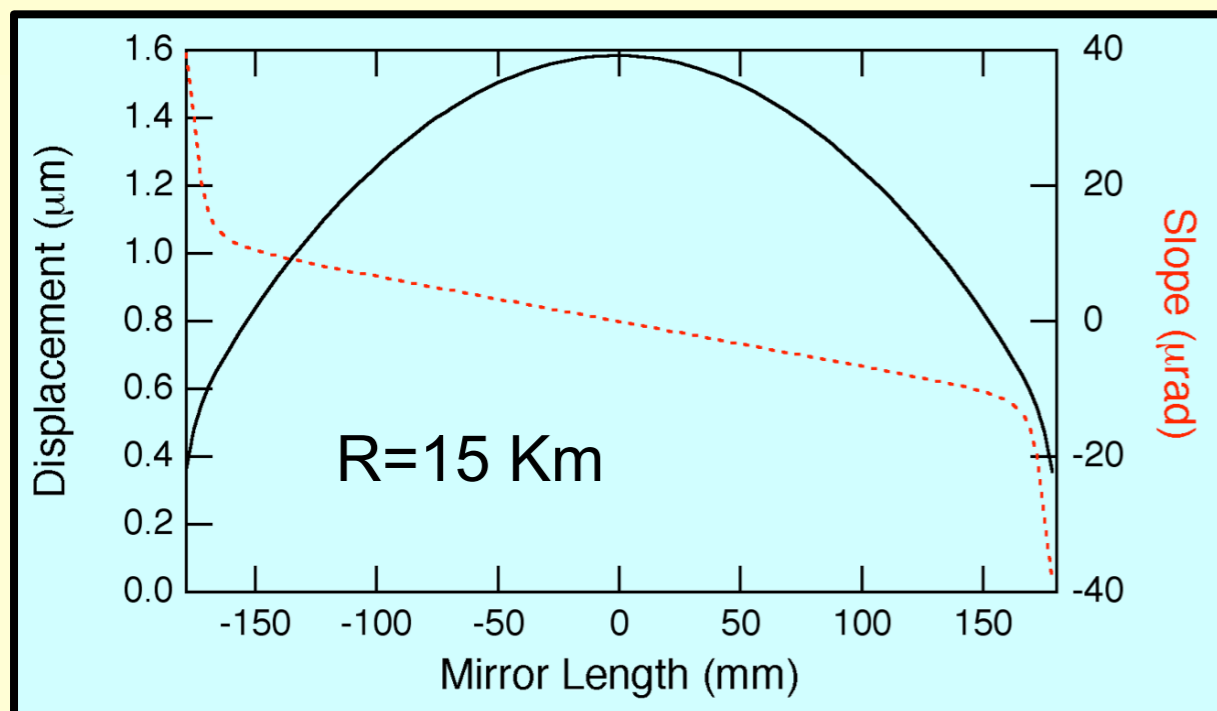
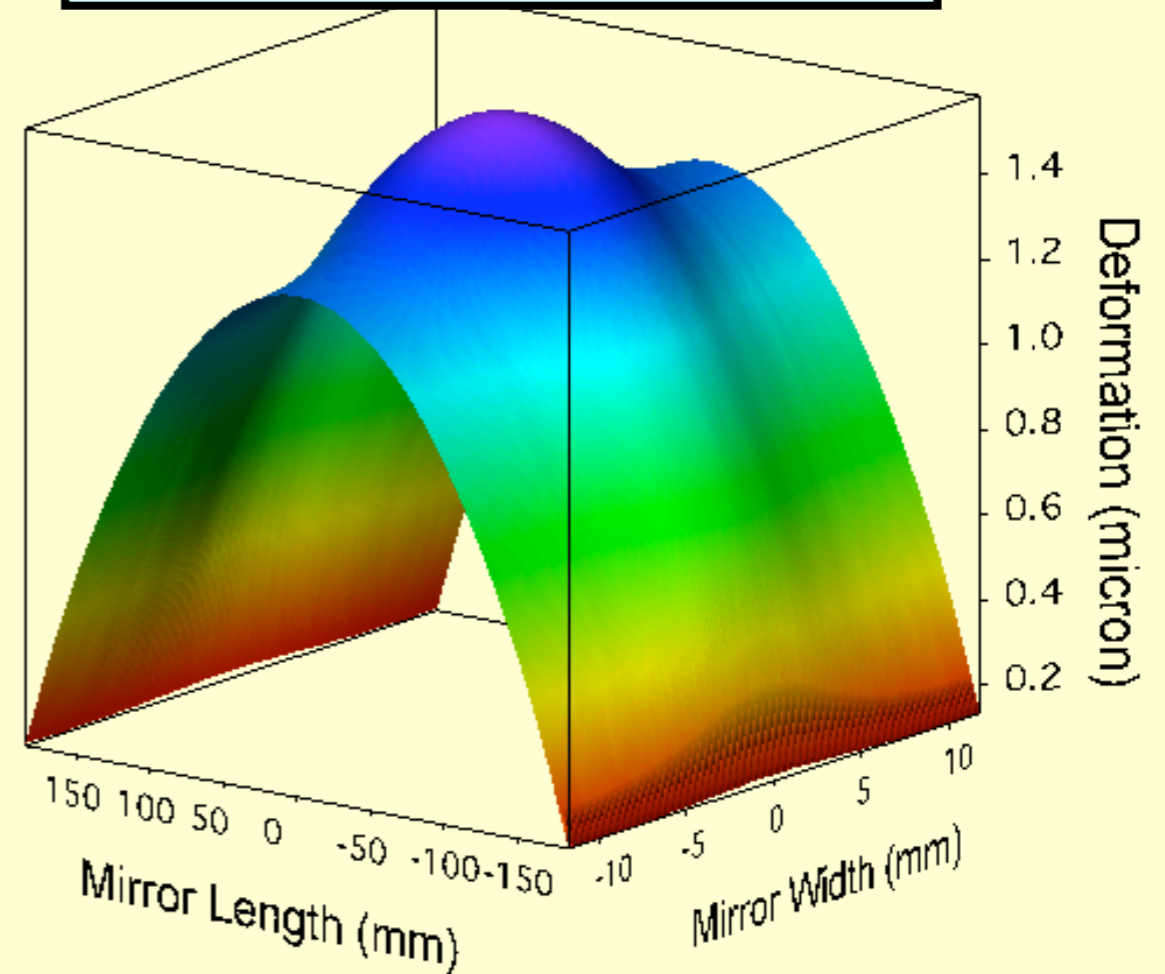


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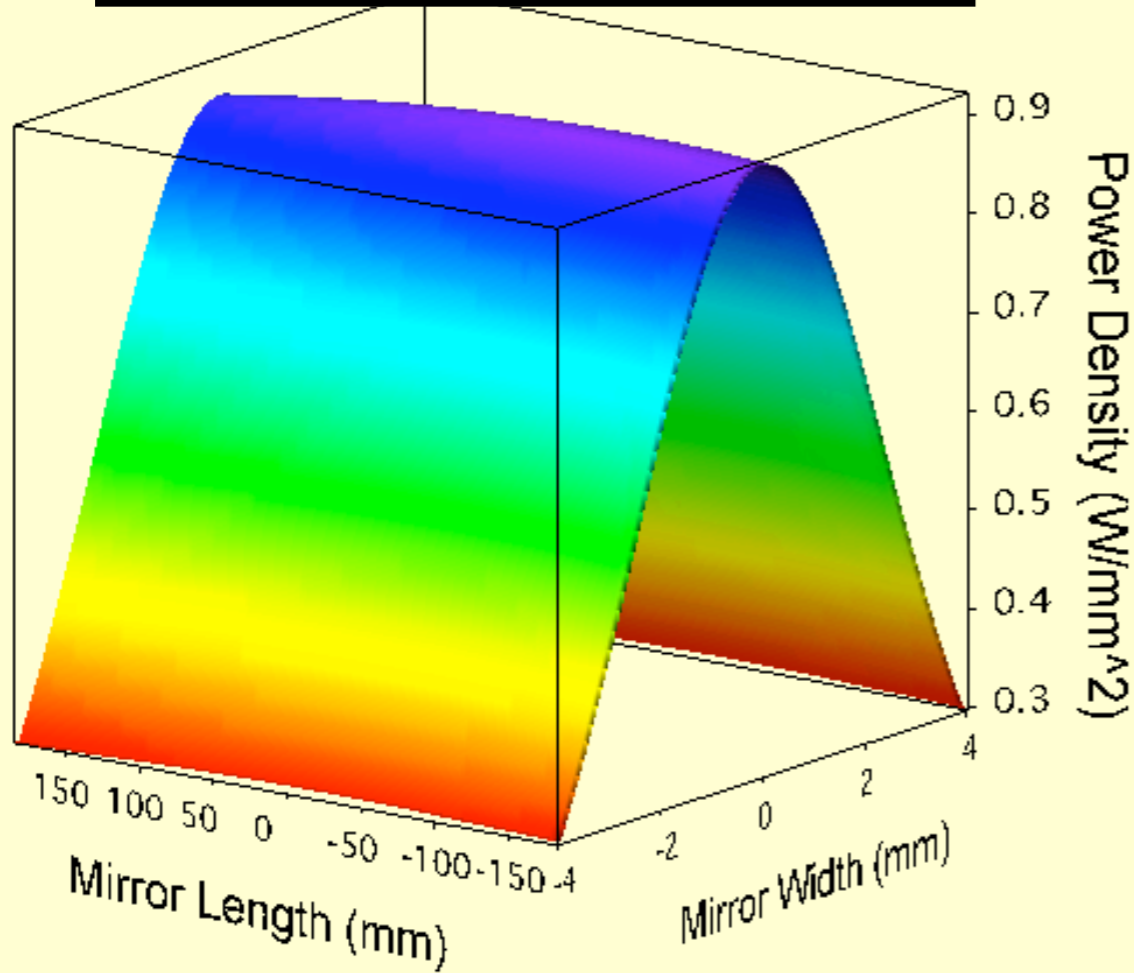
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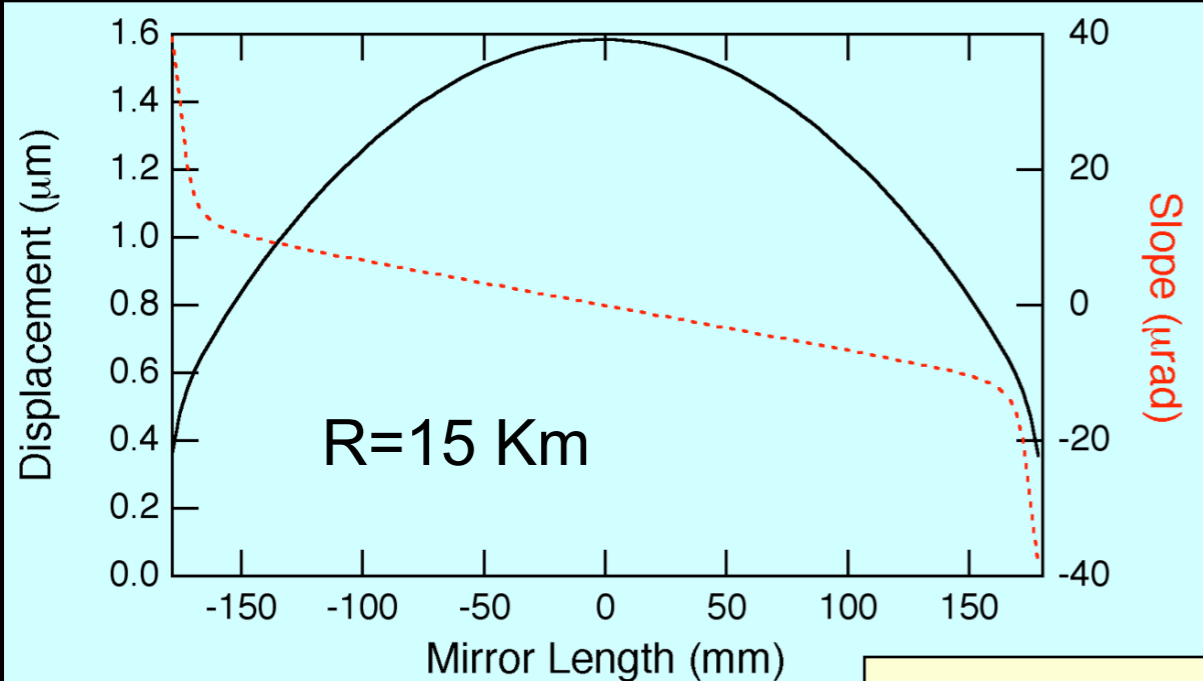
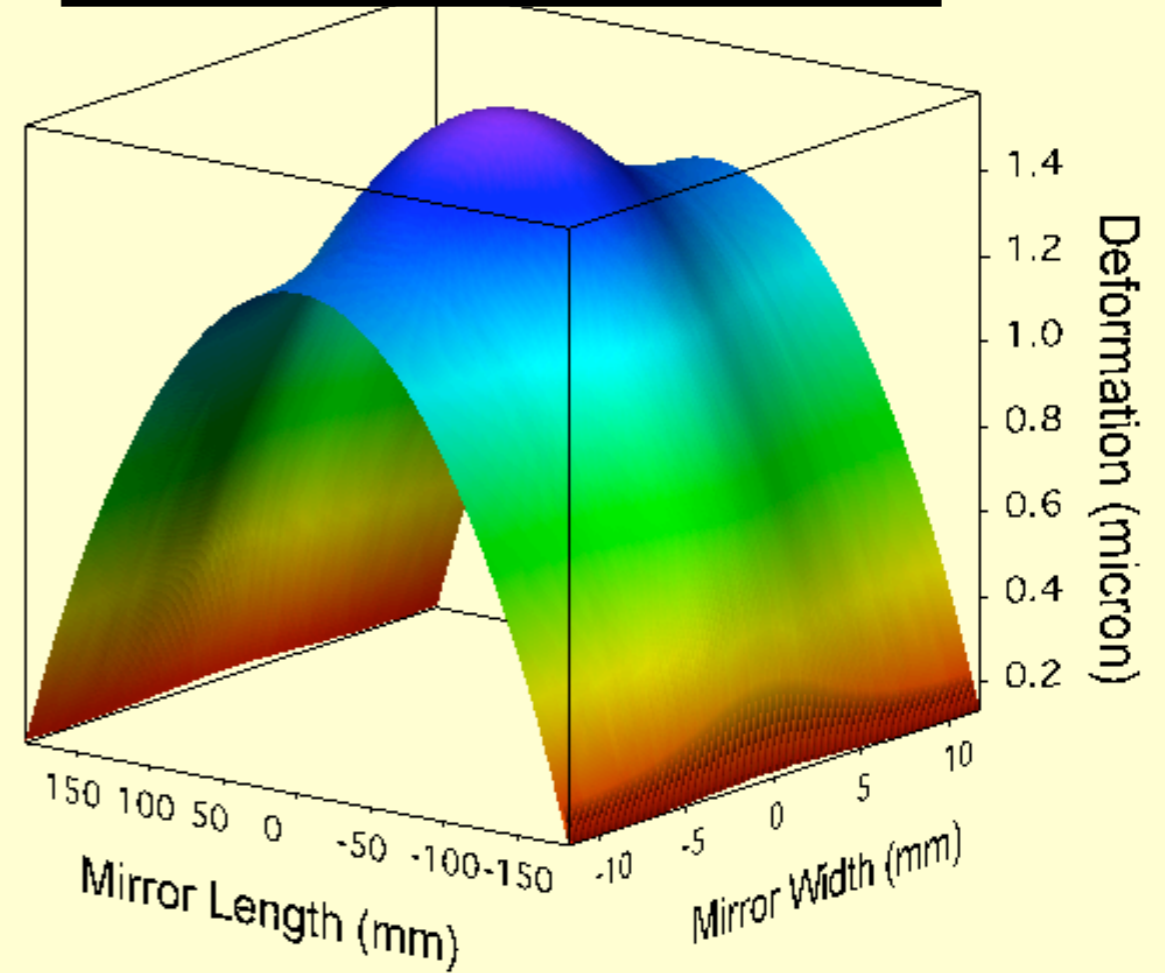
$\rho=1.29$ m 1.32 m

Power on M1

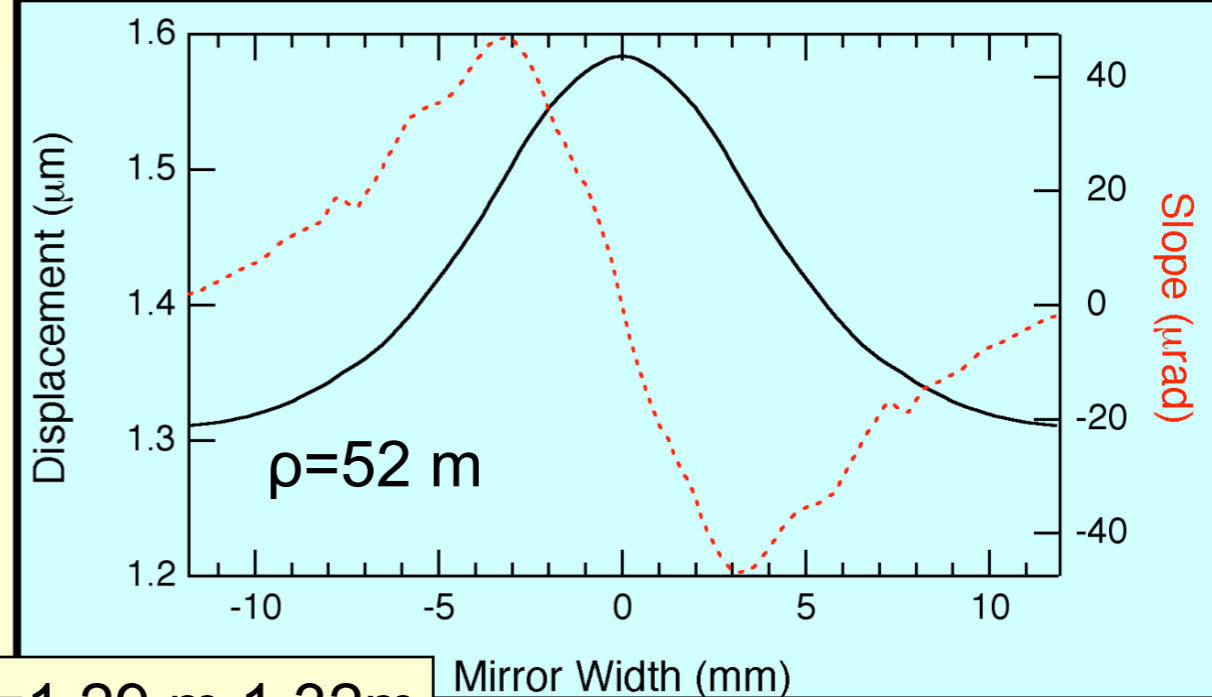
➔ Total absorbed 1.9 kW



➔ Internally water cooled



Acceptance

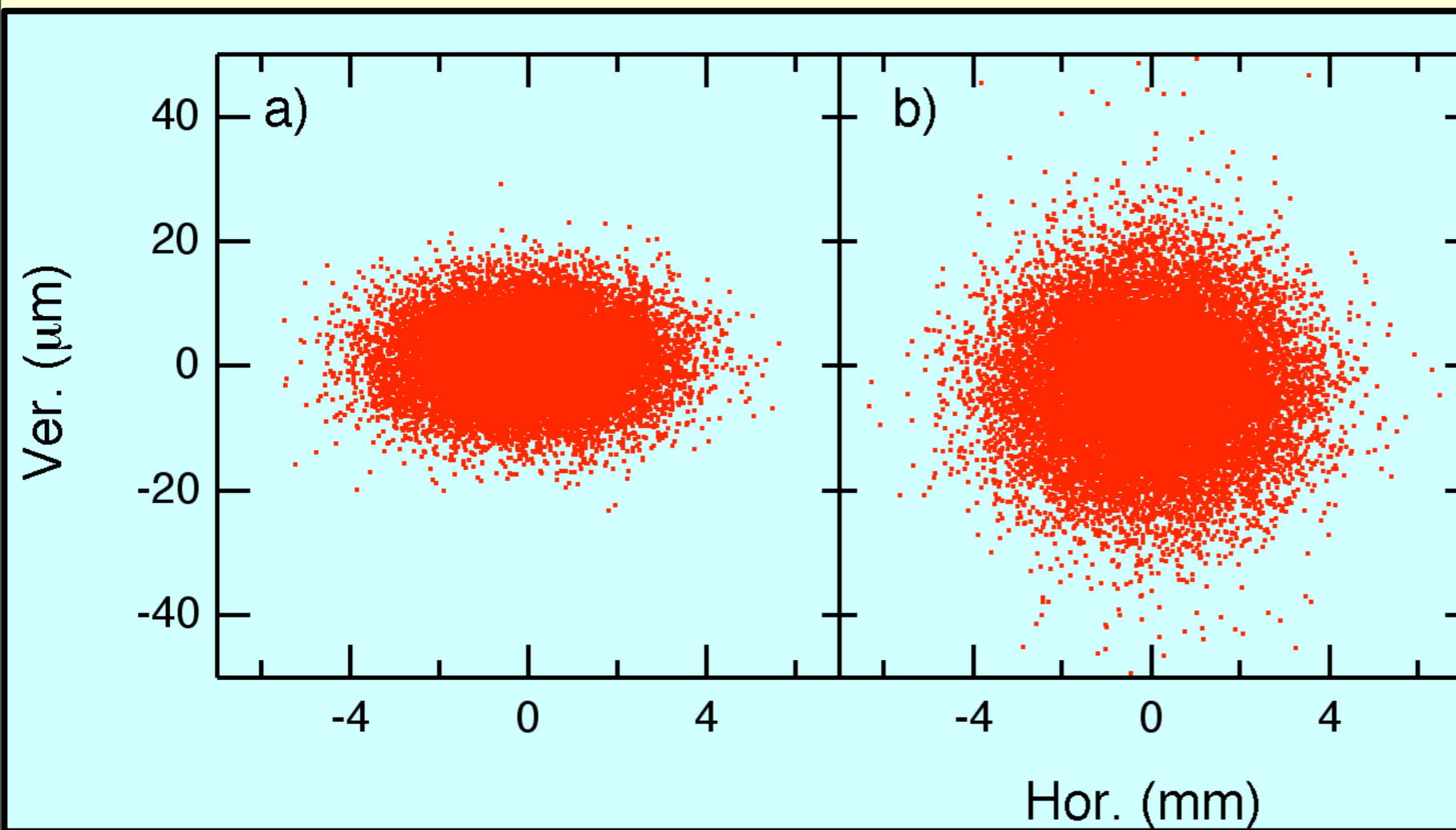


$\rho=1.29$ m 1.32 m

Ray Traces Slit

Ideal

+Heat

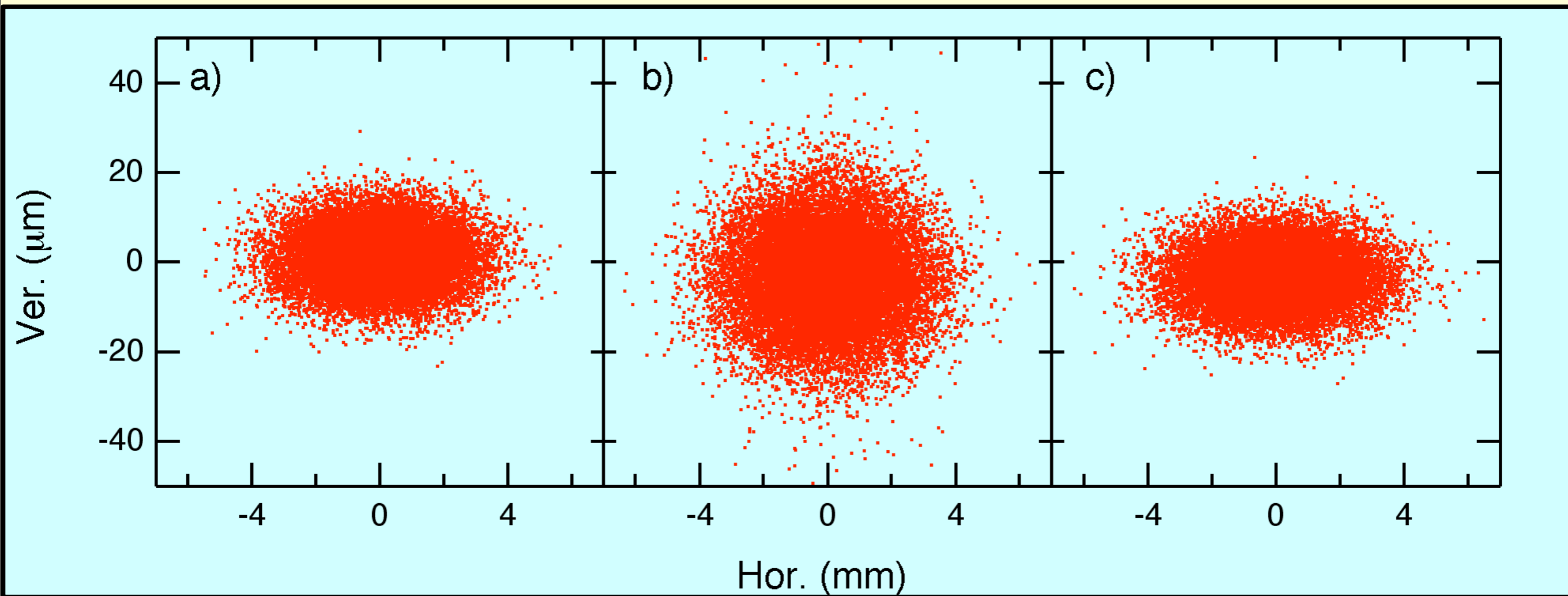


Ray Traces Slit

Ideal

+Heat

+Heat+change c



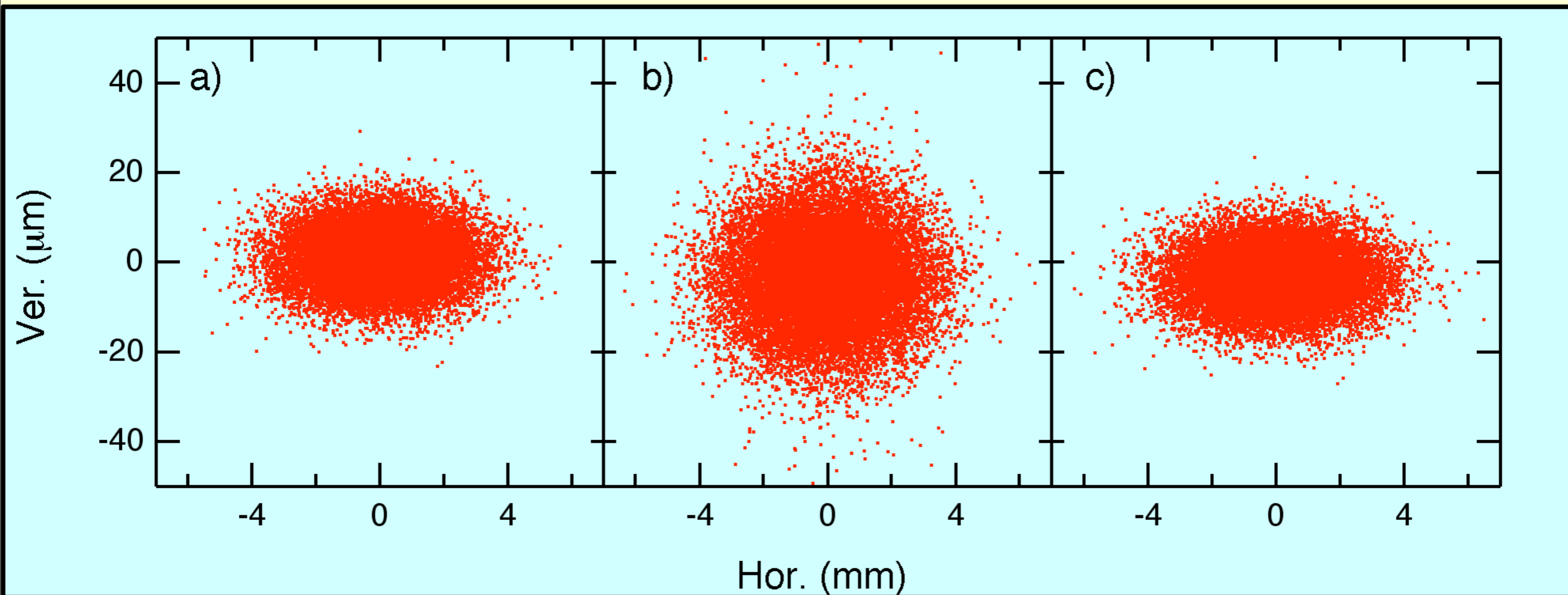
c value
2.183 to 2.201
93% beam

Ray Traces Slit

Ideal

+Heat

+Heat+change c



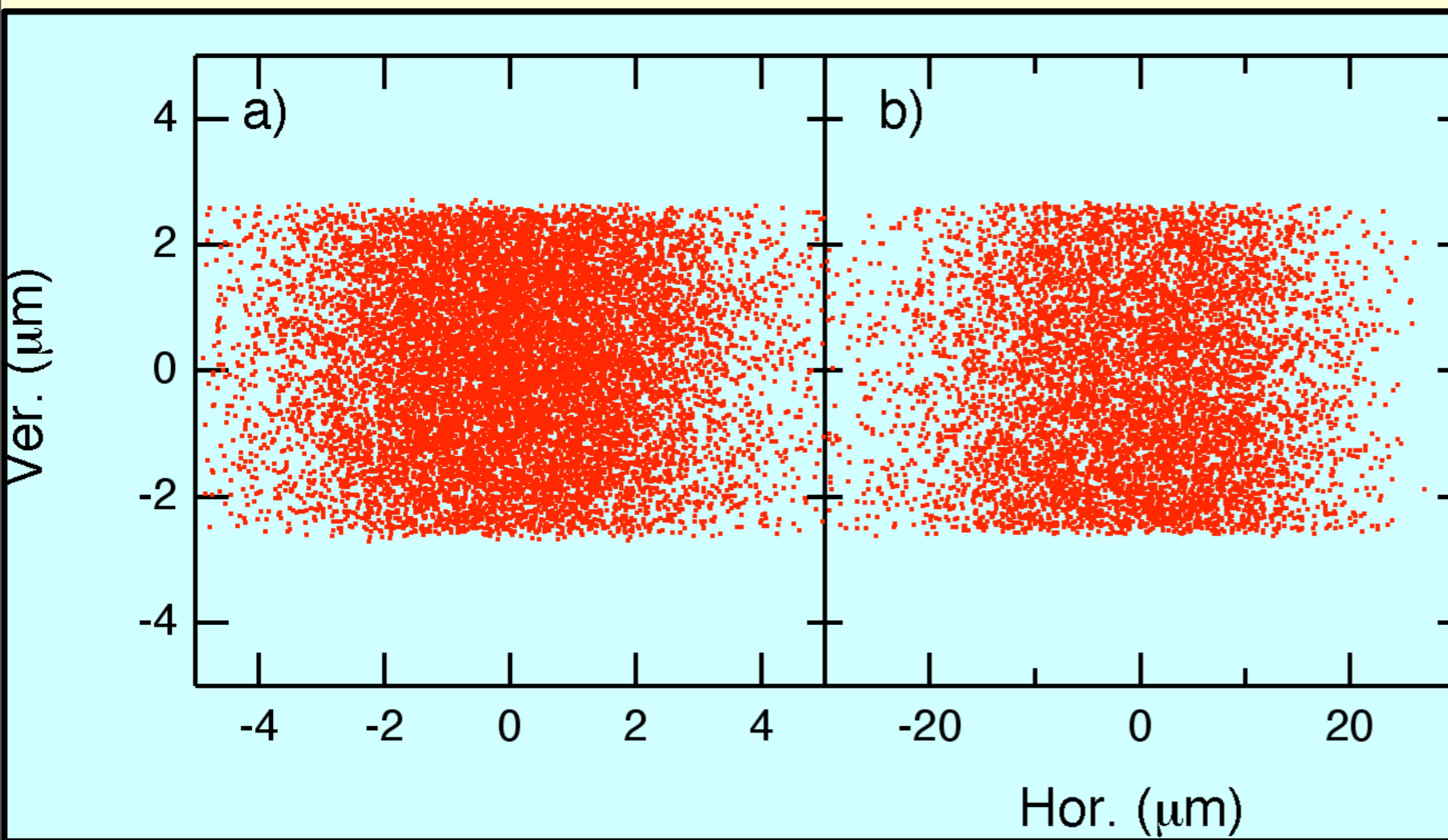
Could be achieved in the collimated PGM by moving slit

c value
2.183 to 2.201
93% beam

Ray Traces Sample

Ideal

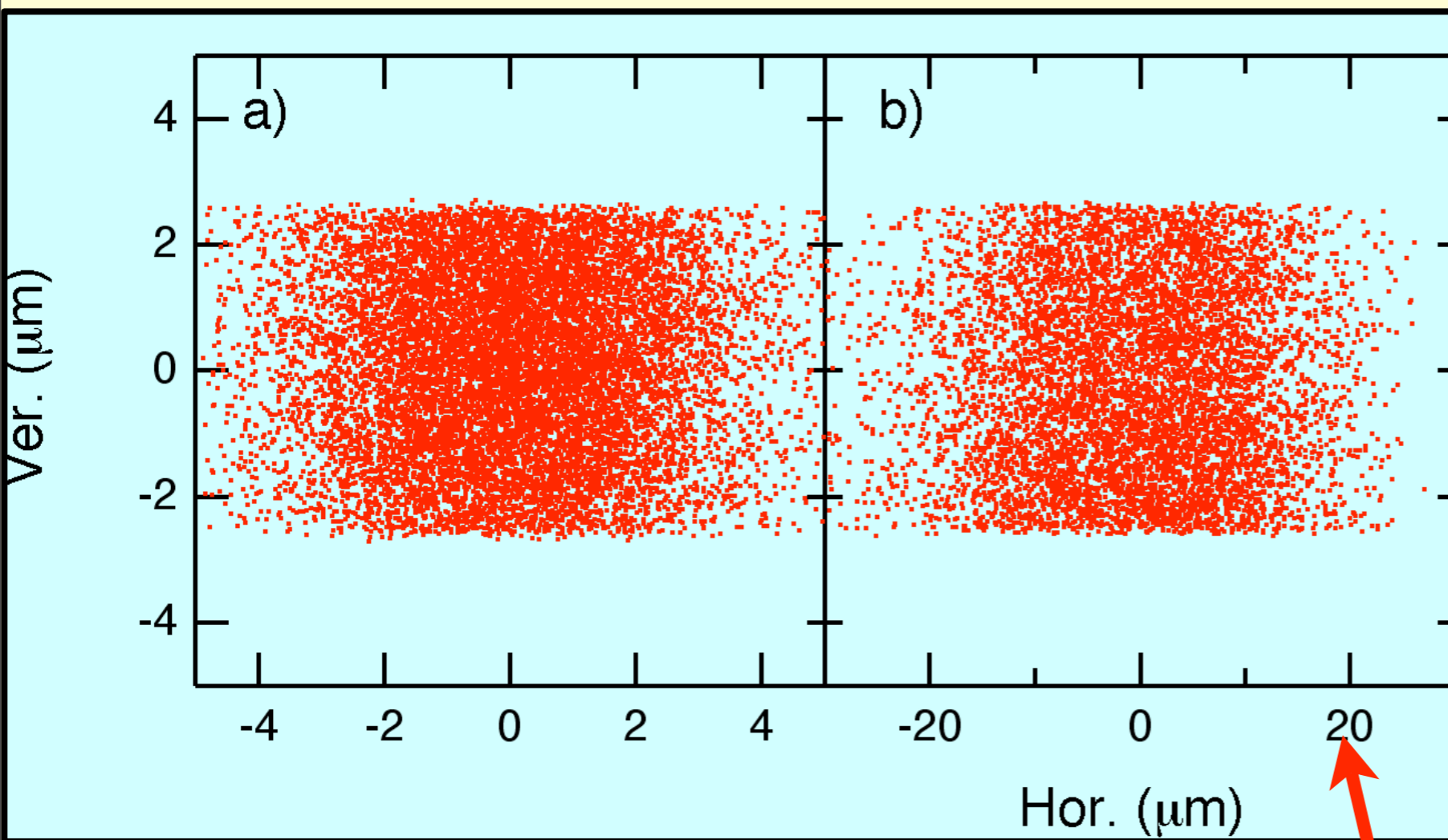
+Heat



Ray Traces Sample

Ideal

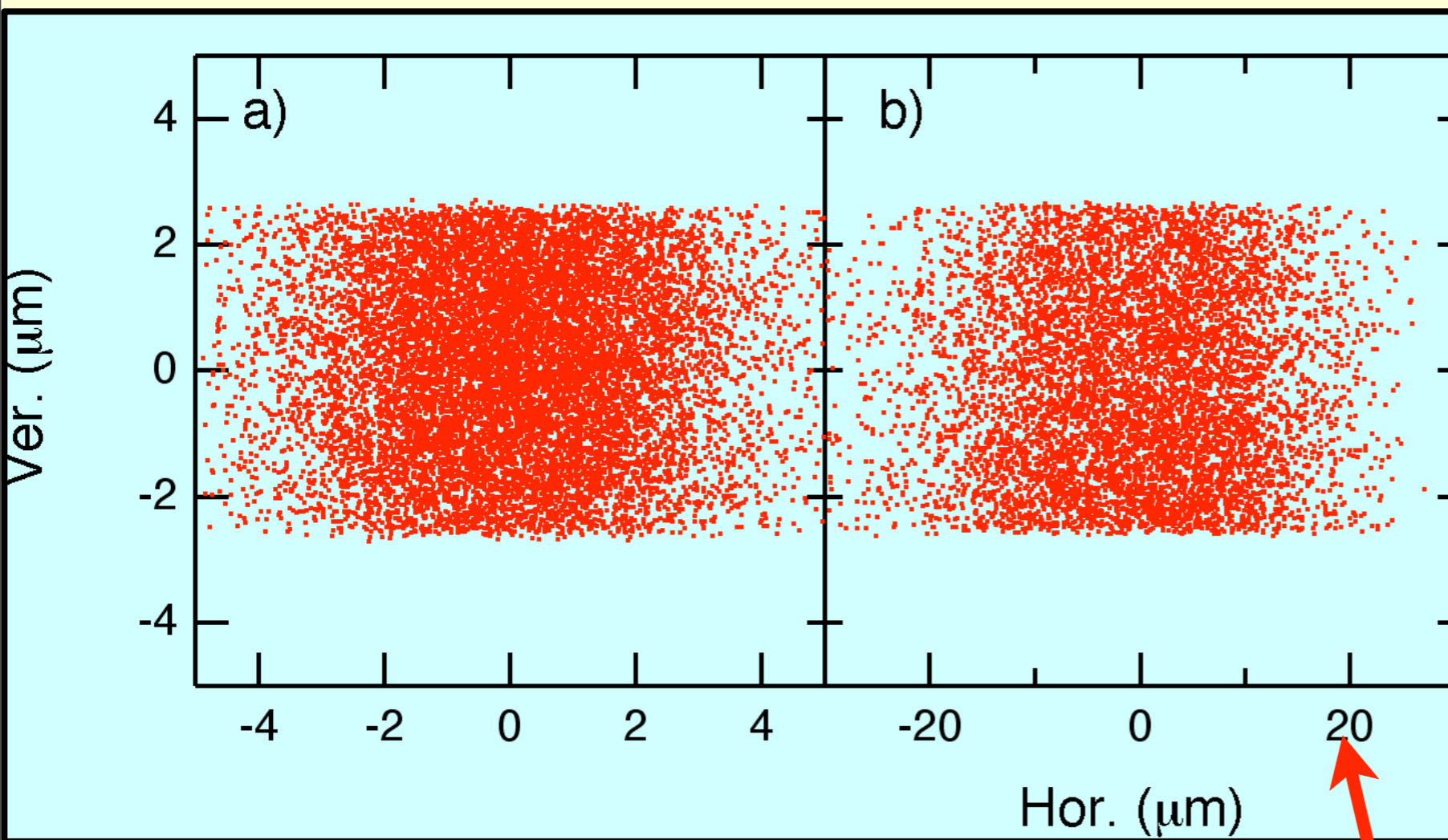
+Heat



Ray Traces Sample

Ideal

+Heat

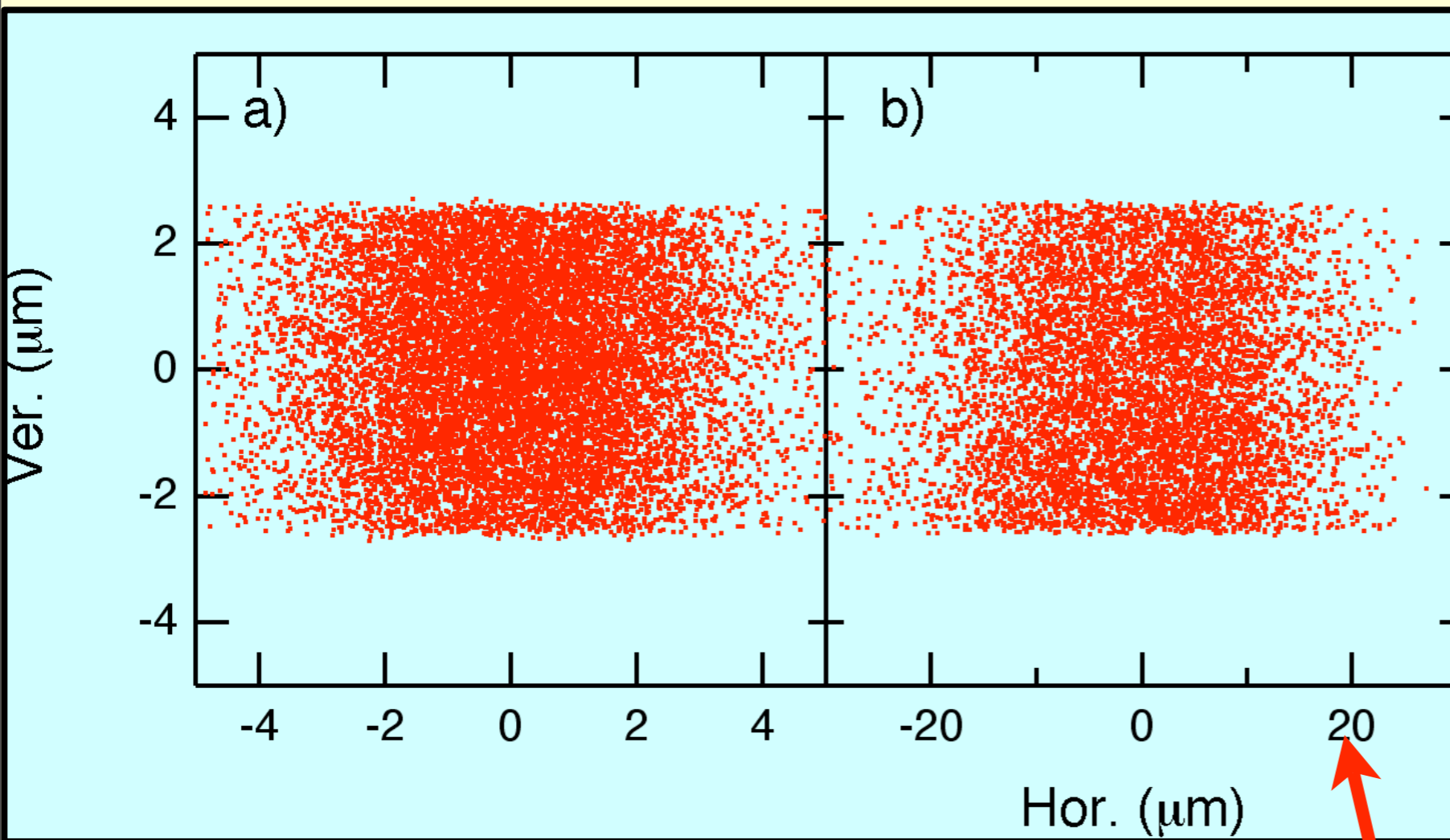


Hor. Source at 43.2 m

Ray Traces Sample

Ideal

+Heat



Hor. Source at 43.2 m

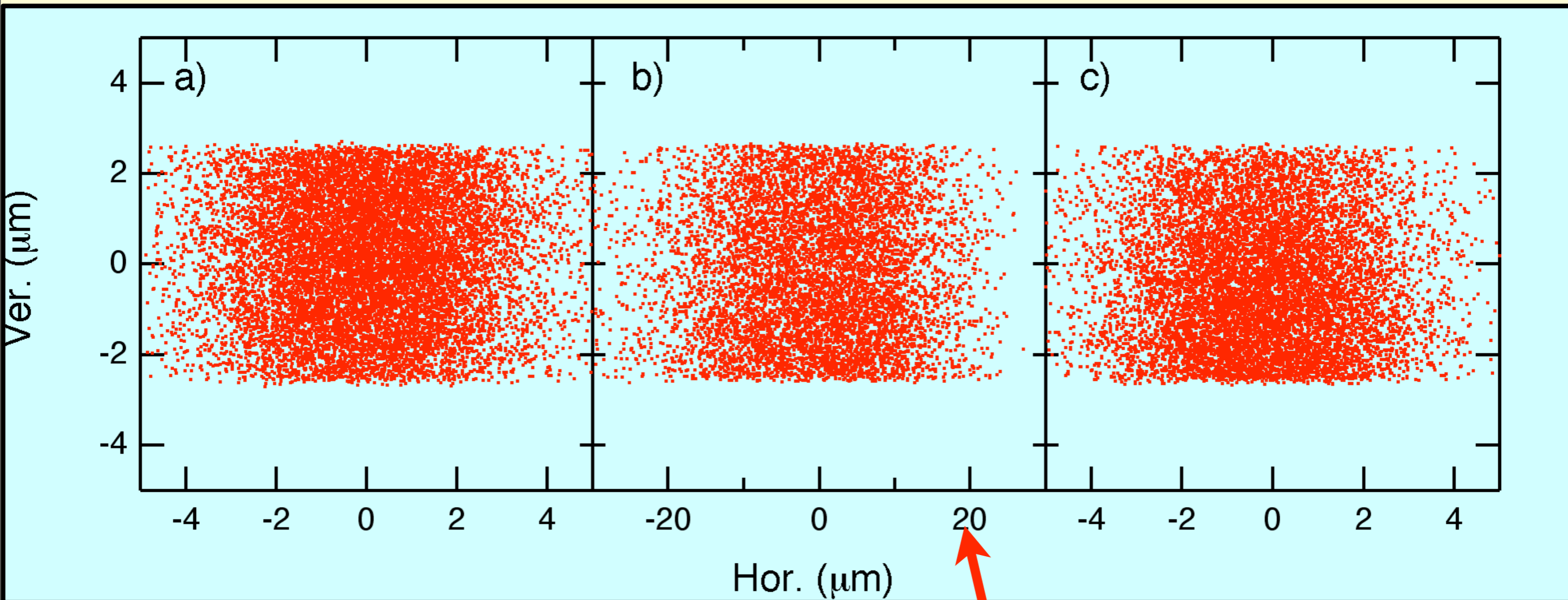
Hor. Source at 37.6 m

Ray Traces Sample

Ideal

+Heat

+Heat+bending mirror



Hor. Source at 43.2 m

Hor. Source at 37.6 m

Will It Work?

- ➔ Resolution recovered by changing c
- ➔ Spot at sample (hor.) by changing M3 (ellip. cyl.)
- ➔ Top-up mode
- ➔ No ID scan or very limited energy range
- ➔ Generate a working table
 - ➔ Gap
 - ➔ Resolution
 - ➔ Spot size
 - ➔ Temperature
- ➔ On line measurements radius curvature and resolution ➔ Real time correction.